

*Second Two-Day Meeting on Internal Combustion Engine Simulations Using the OpenFOAM technology, Milan 26-27<sup>th</sup> November 2016.*



POLITECNICO  
MILANO 1863



# **In-cylinder flows and combustion modeling: application and validation to real and engine- like configurations**

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Politecnico di Milano, Department of Energy

# Topics

In-cylinder flows and combustion modeling using OpenFOAM® technology

OpenFOAM

Lib-ICE

CFD  
methodologies

Validation

Application

Next  
steps...

# Lib-ICE

Internal combustion engine modeling using the OpenFOAM technology

OpenFOAM-x.x.x

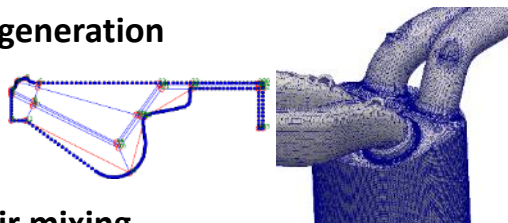
Lib-ICE

**Library:** physical models,  
mesh management

**Applications:** solvers (cold  
flow, SI, Diesel, after-  
treatment), utilities

## Engine simulation workflow

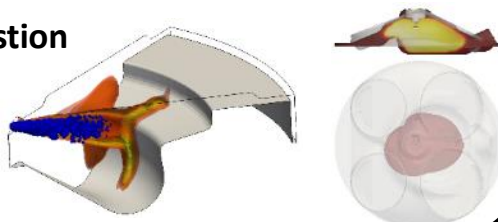
### Mesh generation



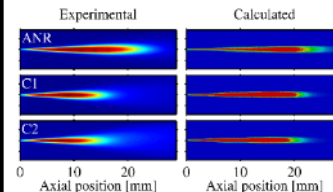
### Fuel-air mixing



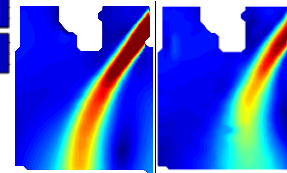
### Combustion



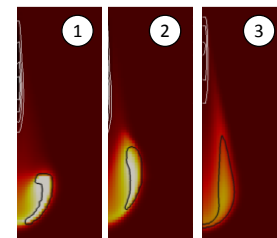
## Development/validation



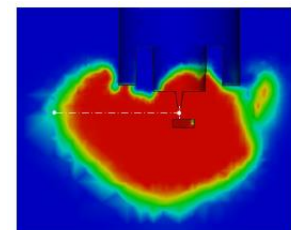
### Spray modeling



### Engine flows



### Diesel combustion



### SI combustion

# Engine simulation workflow

Methodology

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Diesel  
engines

Mesh  
management

Cold flow

Fuel-air  
mixing

Combustion

SI engines

# Engine simulation workflow

## Methodology

Diesel engines

SI engines

Mesh management

Cold flow

Fuel-air mixing

Combustion

- Automatic mesh generation
- Mesh motion
- Topological changes

- Discretization
- Turbulence models
- Mesh quality

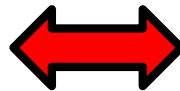
- Lagrangian spray
- Sub-models
- Nozzle flow

- Simplified or detailed kinetics
- Ignition
- Pollutants

# Engine simulation workflow

Methodology

Fully integrated approaches



Open-Source code

Diesel engines

SI engines

Mesh management

Cold flow

Fuel-air mixing

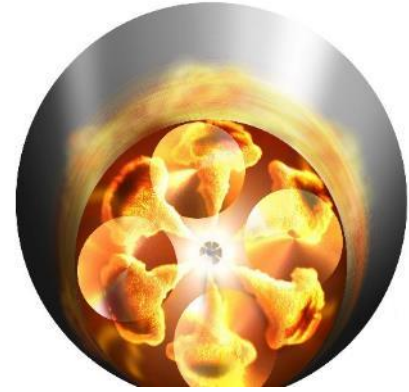
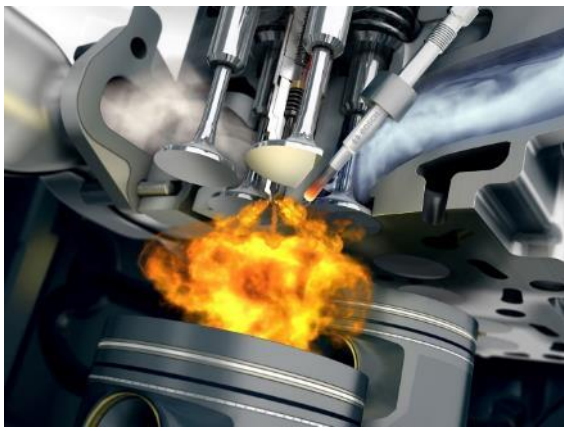
Combustion

- Automatic mesh generation
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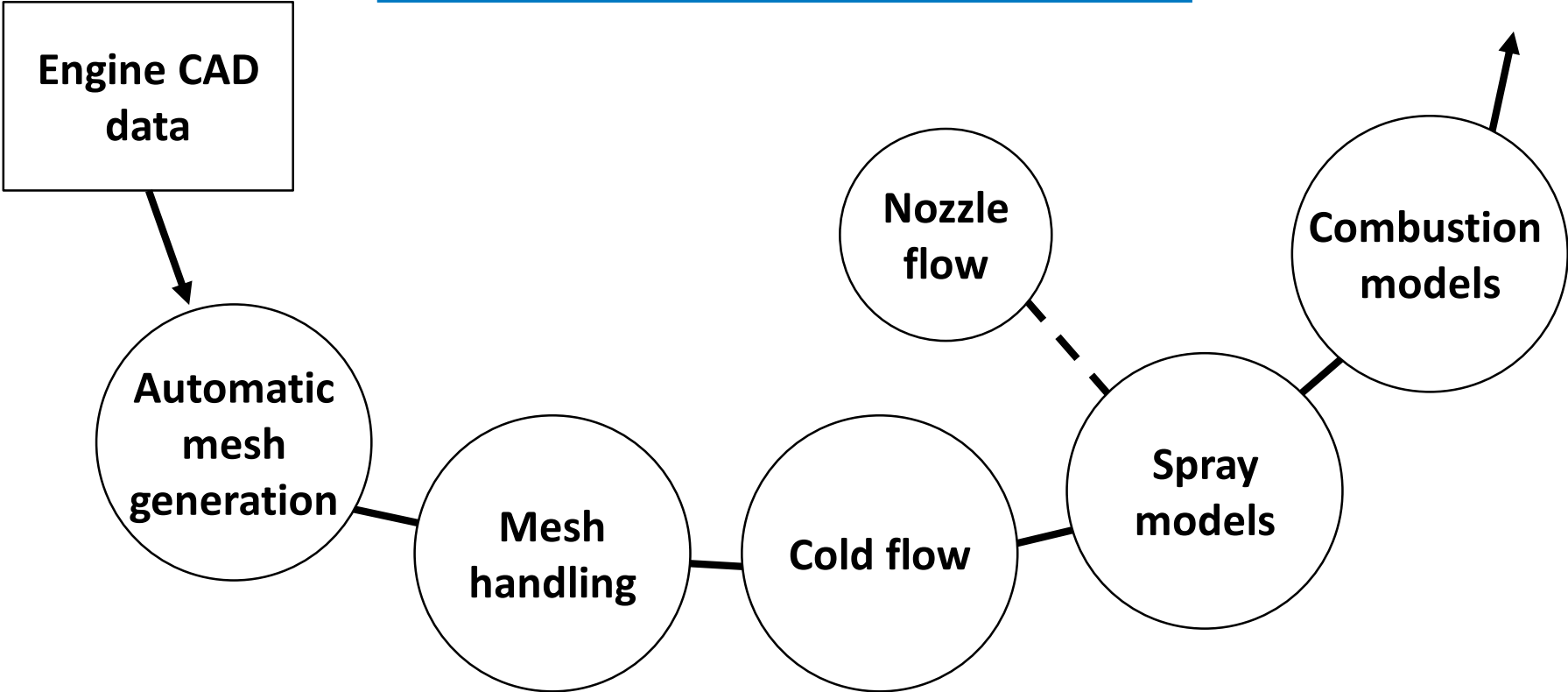


# Diesel Engines



# Diesel engines

Methodology / model development



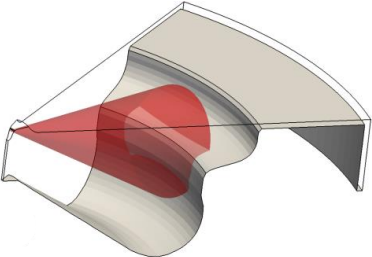


# Diesel engines

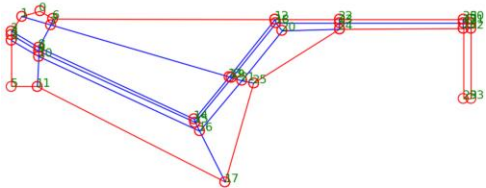
## Mesh management

### Automatic mesh generation

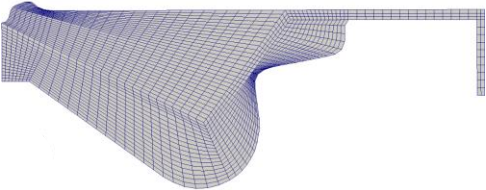
a) Main engine data



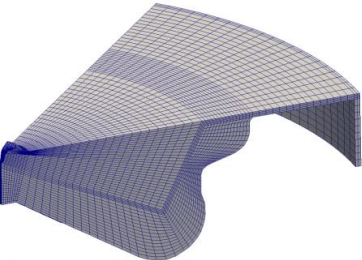
b) Spray oriented block mesh



c) Combustion chamber points fit

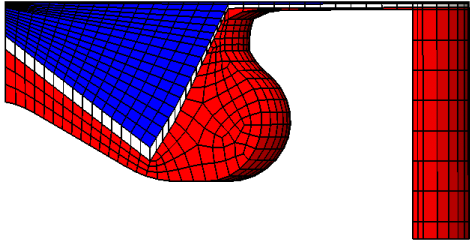


d) Spray-oriented mesh



### Mesh handling

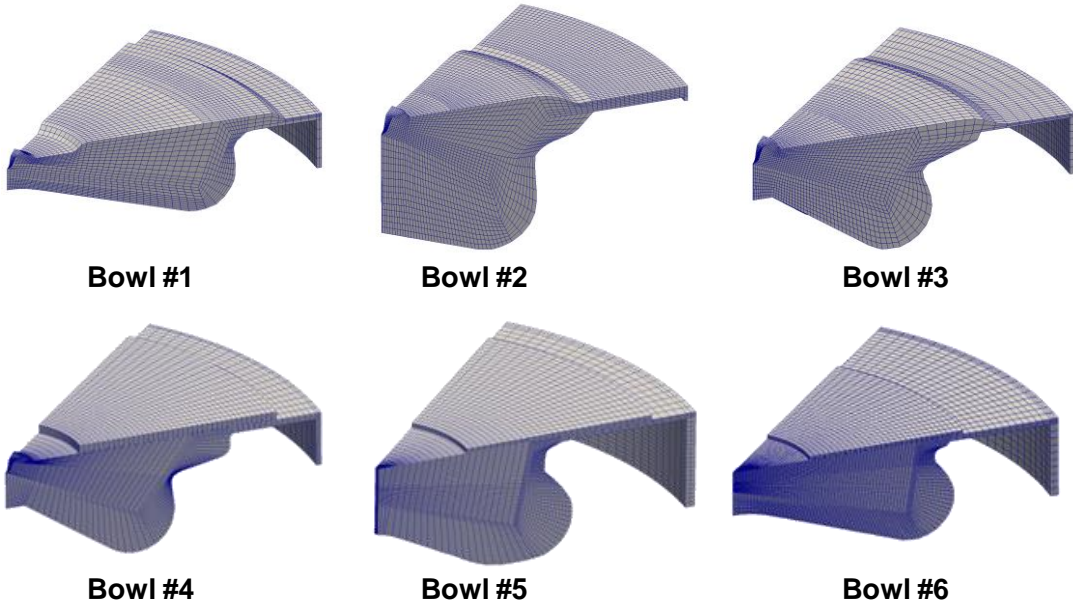
### Dynamic layering



# Diesel engines

## Mesh management

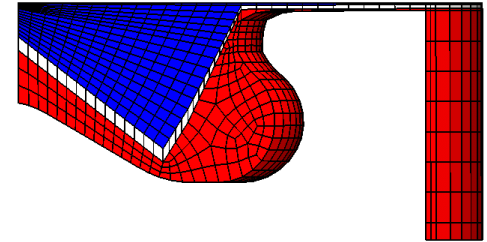
### Automatic mesh generation



From CAD to SIMULATION: 10 minutes

### Mesh handling

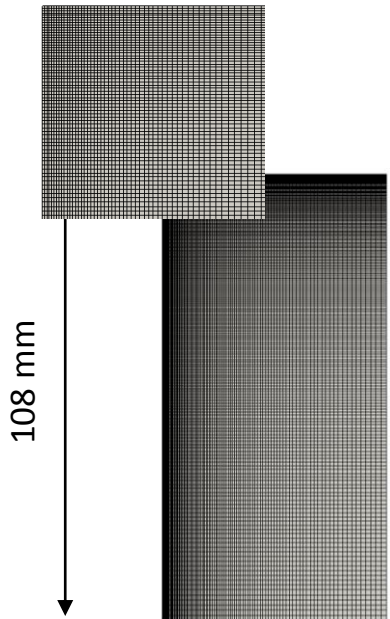
#### Dynamic layering



# Diesel Engines: spray modeling

## Spray A from Engine Combustion Network

### 2d computational mesh



### Spray model setup

- Injection: blob
- Breakup: KHRT
- Evaporation: Spalding

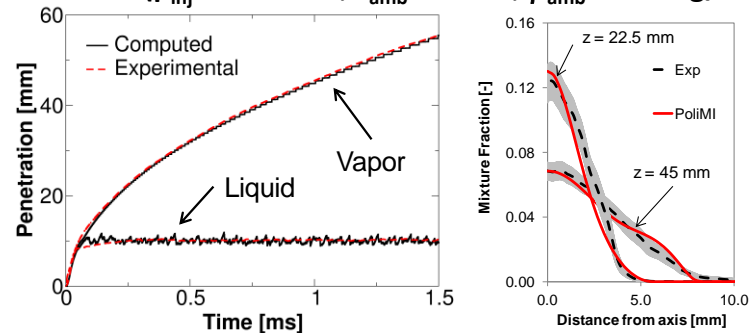
### CFD setup

- Turbulence model: standard  $k-\epsilon$  with modified  $C_1$

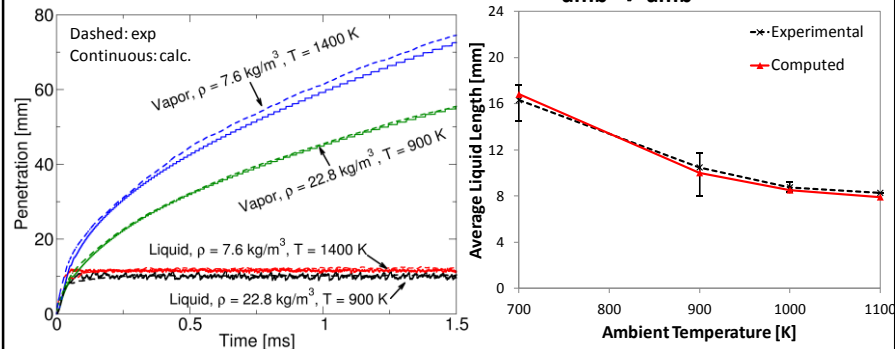
### Test conditions

- Fuel n-dodecane
- Nozzle diameter:  $90 \mu\text{m}$
- $p_{inj}$ : 50-150 MPa
- $T_{amb}$ : 700-1200 K
- $\rho_{amb}$ :  $7.6 - 22.8 \text{ kg/m}^3$

### Baseline ( $p_{inj} = 150 \text{ MPa}$ ; $T_{amb} = 900 \text{ K}$ ; $\rho_{amb} = 22.8 \text{ kg/m}^3$ )



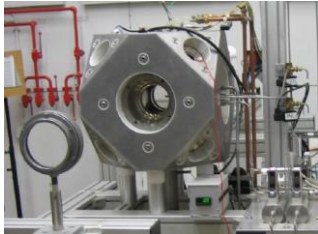
### Parametric variations ( $T_{amb}$ , $\rho_{amb}$ )



# Diesel Engines: spray modeling

FPT C11 Spray (collaboration with TU/e – DI N. Maes and Prof. B. Somers, FPT support)

## TU/e optical vessel



- Liquid penetration: DBI
- Vapor penetration: Schlieren

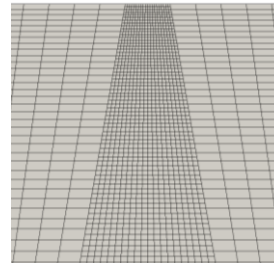
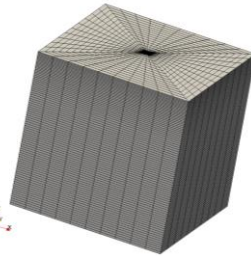
## Operating conditions

- Nozzle diameter: 0.205 mm
- Ambient temperature: 900 K

	ANR	C1	C2
$P_{inj}$ [MPa]	150	80	150
$\rho_{amb}$ [kg/m <sup>3</sup> ]	22.8	40	40

## CFD Setup

### 3D mesh



- Consistent with the engine grid in size and structure

### Spray

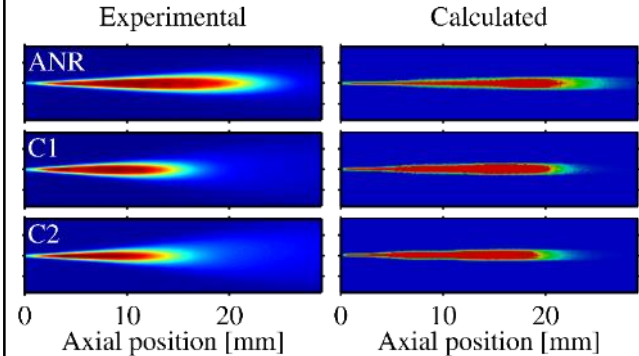
- Huh-Gosman atomization
- Pilch-Erdman breakup

### Turbulence modeling

- $k-\epsilon$  with modified  $C_1$

## Validation

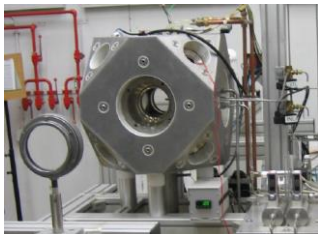
- Liquid: exp vs computed extinction profiles



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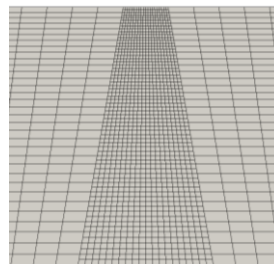
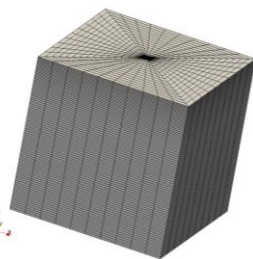
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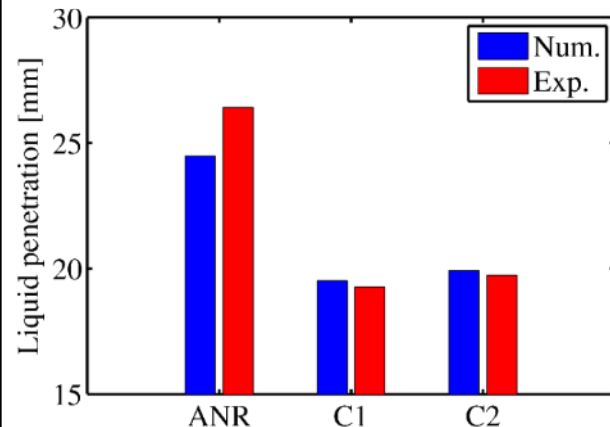
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### Turbulence modeling

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## Validation

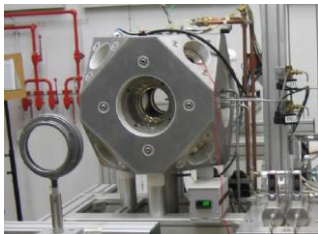
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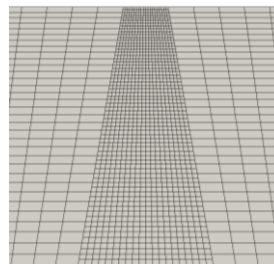
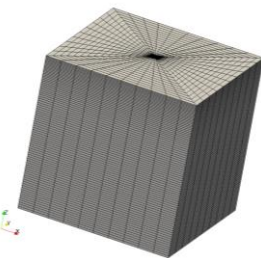
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### 3D mesh



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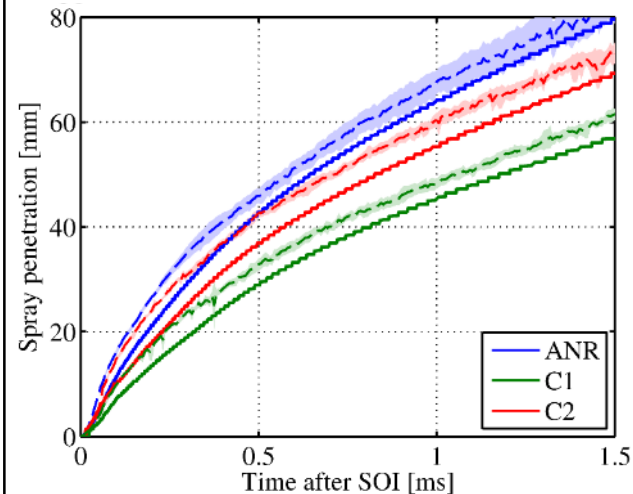
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### Turbulence modeling

- $k-\varepsilon$  with modified  $C_1$

## Validation

- Liquid: exp vs computed extinction profiles



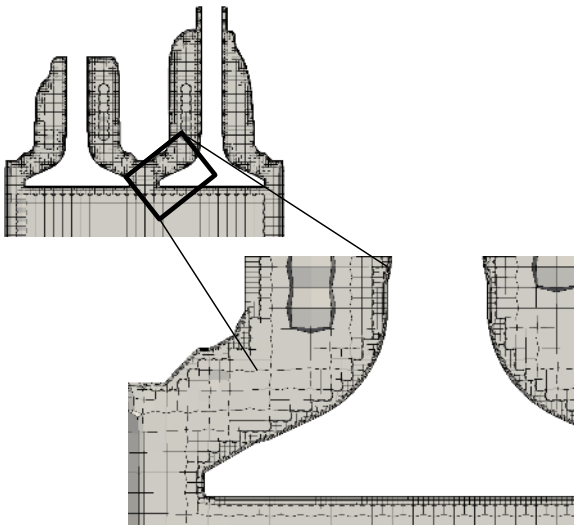
- Vapor: exp (Schlieren), calc. (mixture fraction threshold)



# Diesel Engines: cold flow

Steady state flow bench simulations (FPT Industrial, Gilles Hardy)

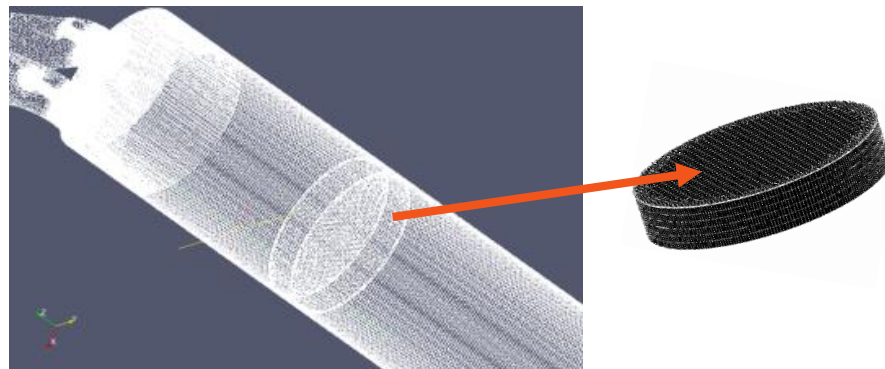
## Mesh generation



Cartesian, body fitted grids with boundary layer generated with cartesianMesh (cfMesh) or snappyHexMesh (OpenFOAM)

## CFD Setup

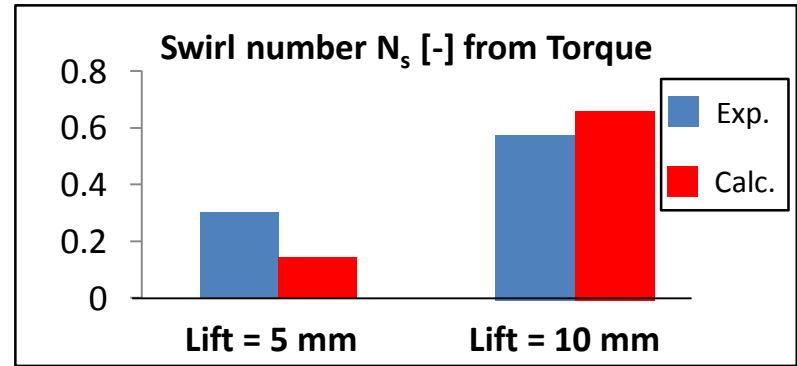
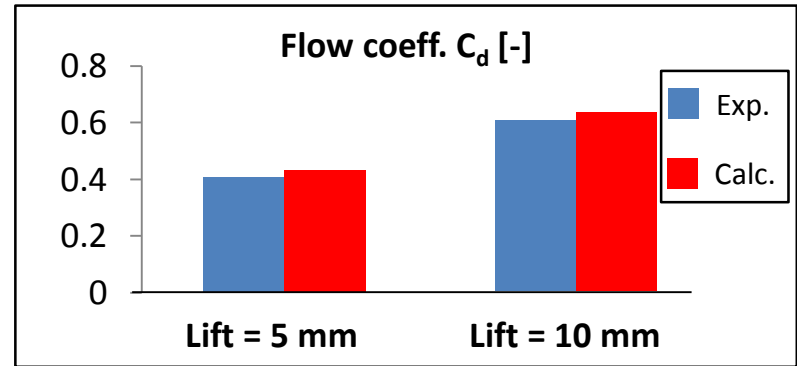
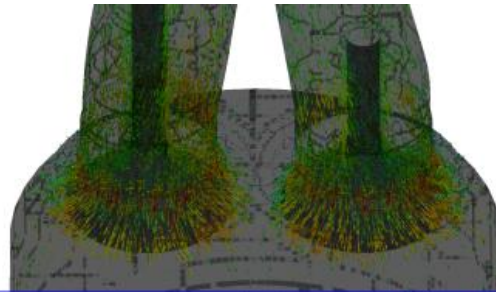
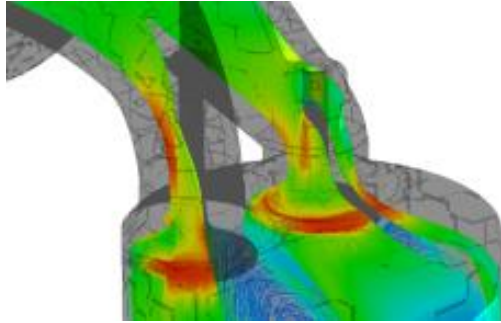
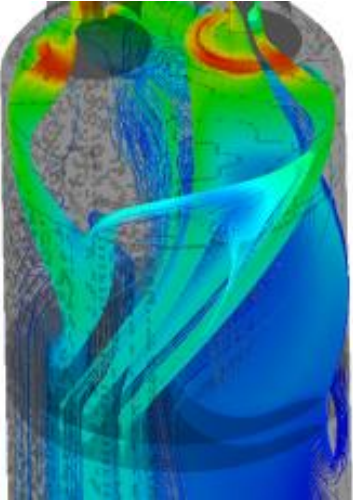
- Steady-state flow
- Turbulence model: standard  $k-\varepsilon$
- Porous media acts as a flow straightener in the computational mesh: computation of the swirl torque
- Verification of angular momentum conservation across the mesh boundaries.



# Diesel Engines: cold flow

Steady state flow bench simulations (FPT Industrial, Gilles Hardy)

Computed flow field

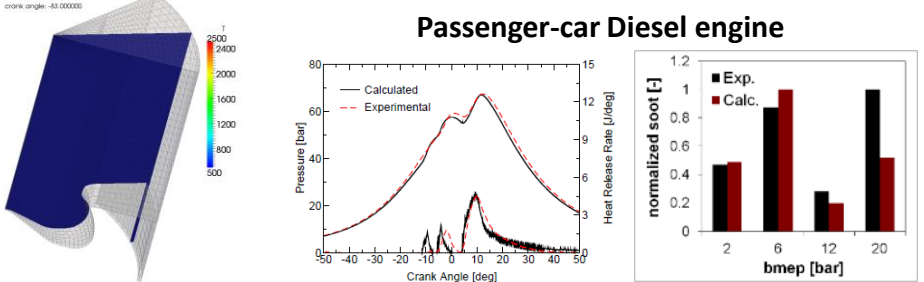




# Diesel Engines

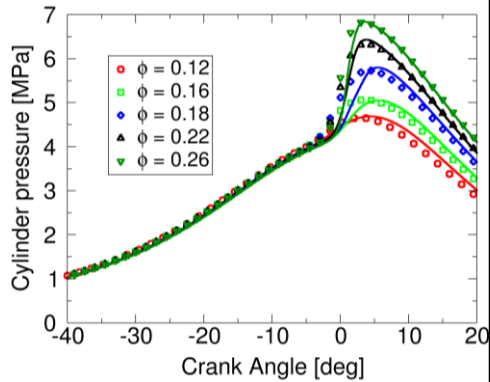
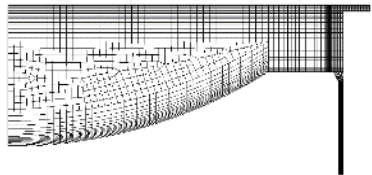
## Combustion modeling

### Characteristic time-scale model (CTC)



### Well-mixed model

Medium-duty engine operating at low-load with iso-octane fuel.

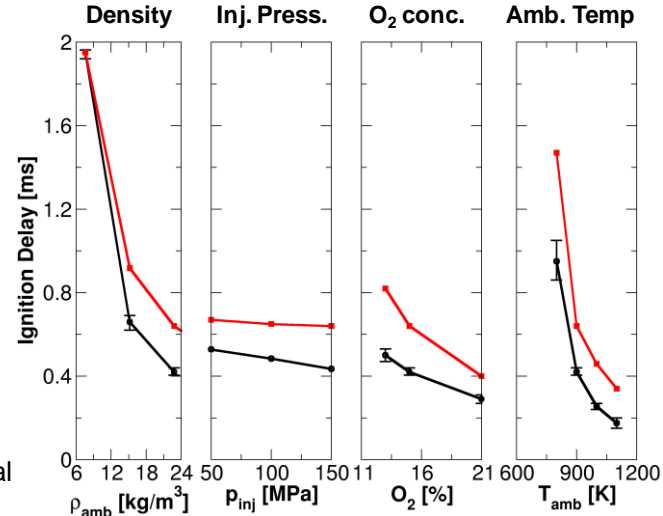


### mRIF model

- N-dodecane spray combustion at constant volume conditions
- ECN Spray-A experiment
- Variation of ambient temperature, density, oxygen and injection pressure
- Kinetic mechanism: Luo et al. (111 species, 467 reactions)

### Ignition delay

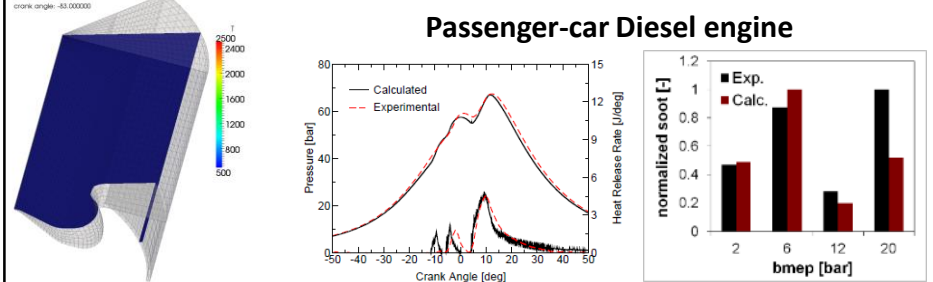
- Computed
- Experimental



# Diesel Engines

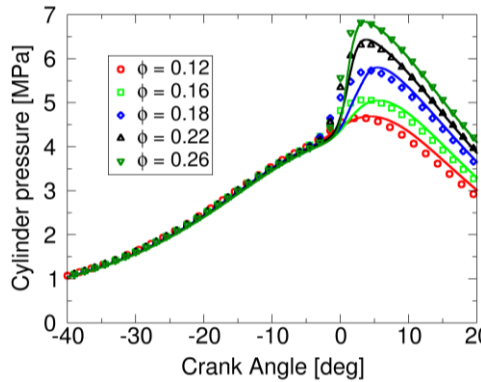
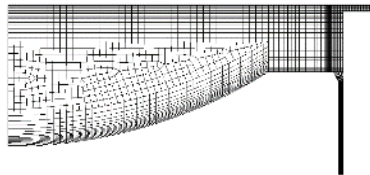
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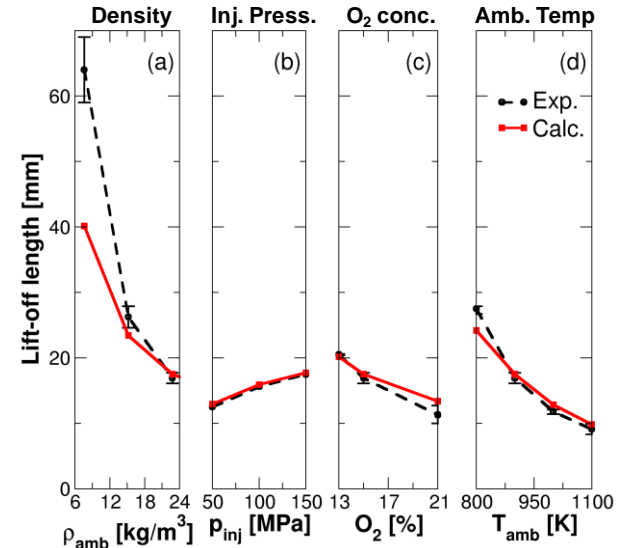


### mRIF model

- N-dodecane spray combustion at constant volume conditions
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- Variation of ambient temperature, density, oxygen and injection pressure
- Kinetic mechanism: Luo et al. (111 species, 467 reactions)

### Flame lift-off

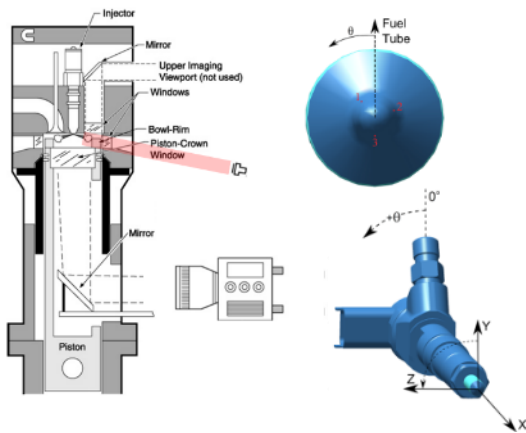
- Computed (red line with squares)
- Experimental (black line with circles)



# Diesel Engines: validation

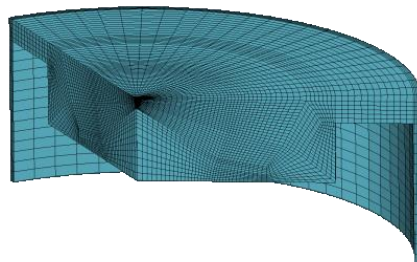
Spray B in Engines (from ECN, collaboration with Dr. Eagle, Dr. Malbec, Dr. Musculus)

## Optically accessible engine with three hole injector



Nozzle design very similar to spray A: possibility to perform same studies in engine and constant-volume vessel.

## CFD setup and tested points



- Same CFD setup used in Spray A simulations, two different combustion models tested: mRIF and well-mixed.

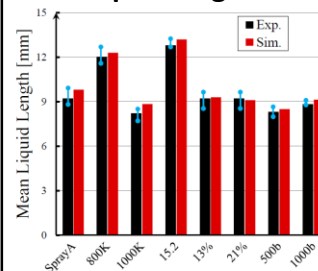
## Tested conditions

- $T@SOI$ : 800-1000 K
- $P_{inj}$  [bar]: 500 – 1500 bar
- $O_2$  [%]: 13-21 %
- $\rho @ SOI$ : 15.2 – 22.8 kg/m<sup>3</sup>

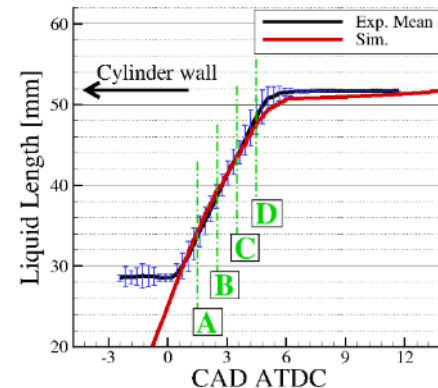
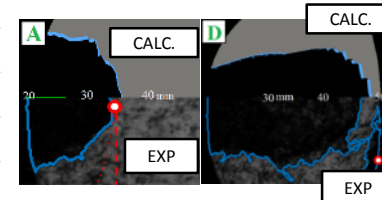
Fuel: n-dodecane

## Validation: non reacting

### Liquid length



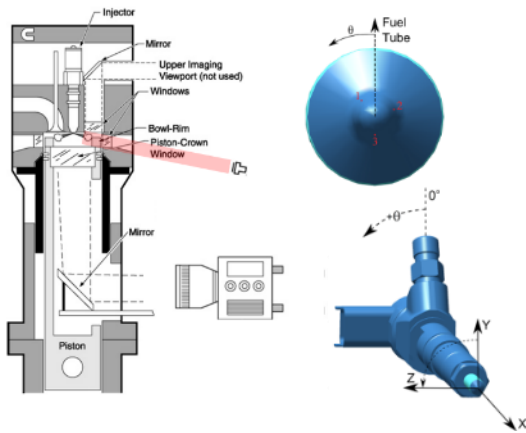
### Vapor distribution



# Diesel Engines: validation

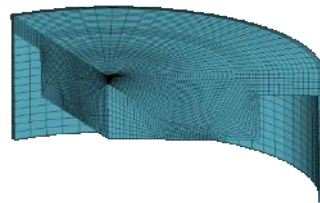
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## Optically accessible engine with three hole injector



Nozzle design very similar to spray A: possibility to perform same studies in engine and constant-volume vessel.

## CFD setup and tested points



Automatically generated grid

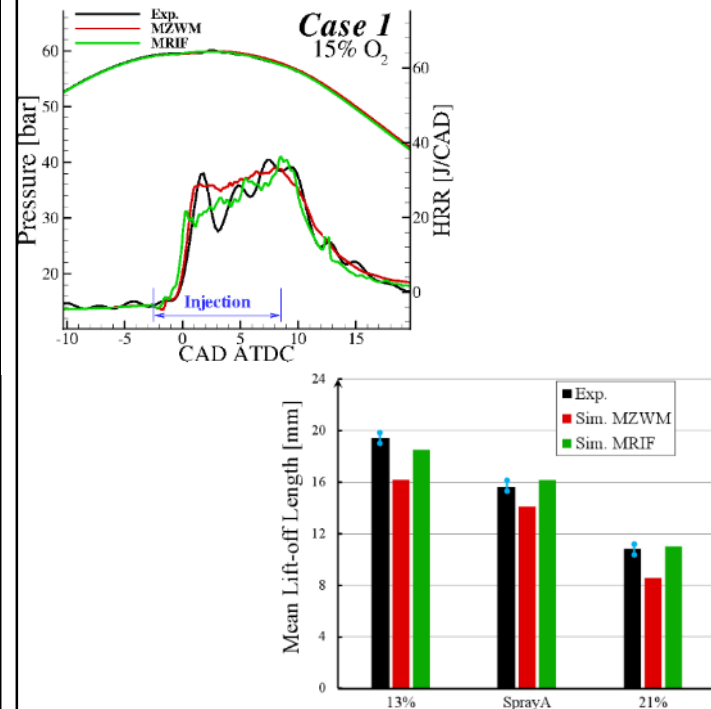
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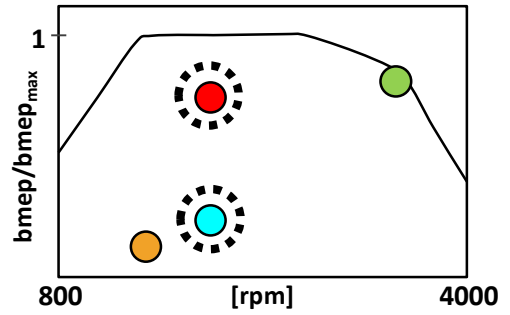
## Validation: reacting



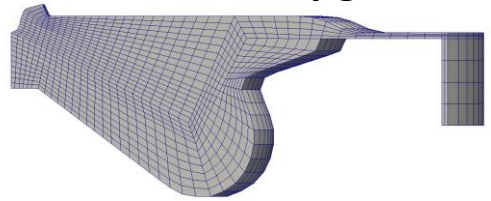
# Diesel Engines: validation

EU 6 FPT Engine MD (support from FPT, DI Gilles Hardy)

Five operating points: with different EGR levels



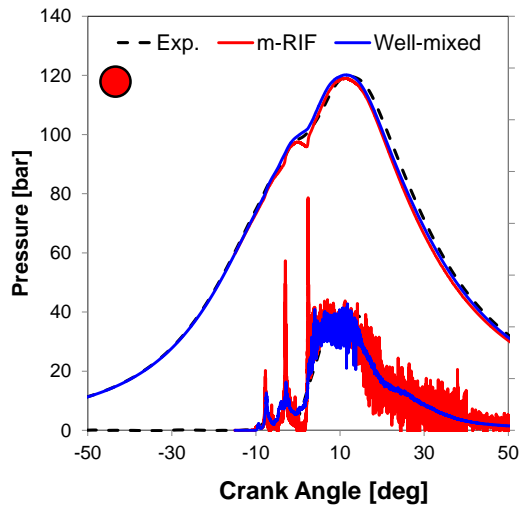
Grid automatically generated



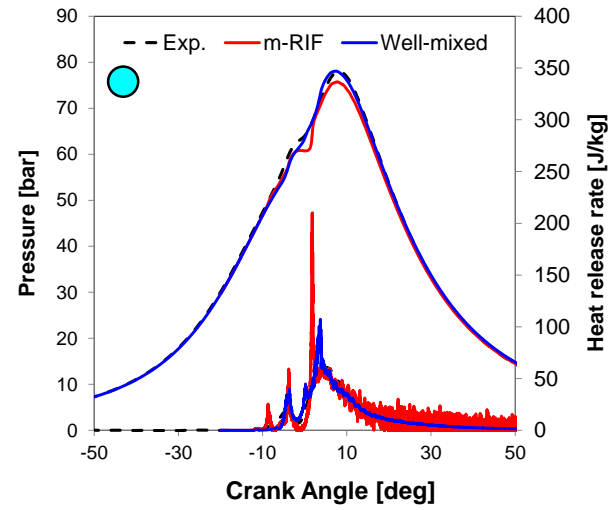
- Initial conditions from 1D simulations

Cylinder pressure validation (mRIF and well-mixed)

75% load, 15% EGR, 2 injections



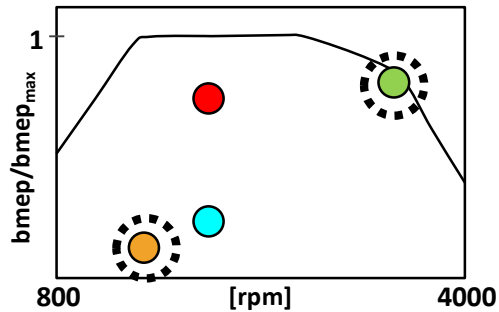
25% load, 20% EGR, 3 injections



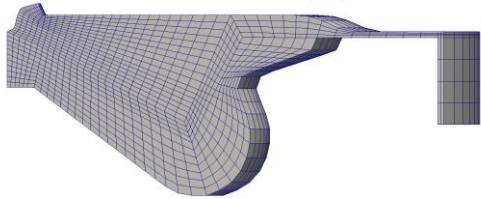
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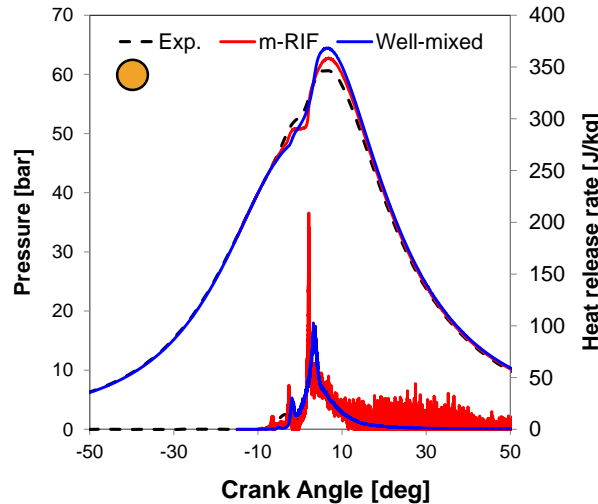
Grid automatically generated



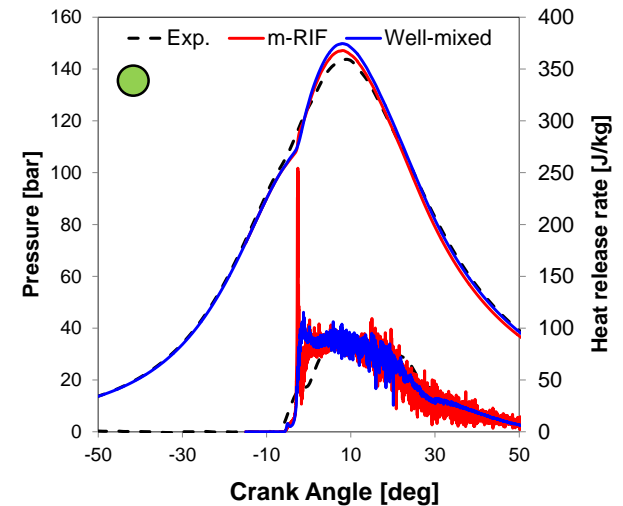
- Initial conditions from 1D simulations

Cylinder pressure validation (mRIF and well-mixed)

10% load, 35% EGR, 3 injections



Full load, 0% EGR, 1 injection



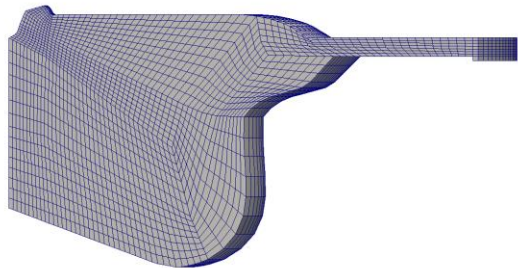
# Diesel Engines: validation

PCCI engine (support from FPT, DI Gilles Hardy)

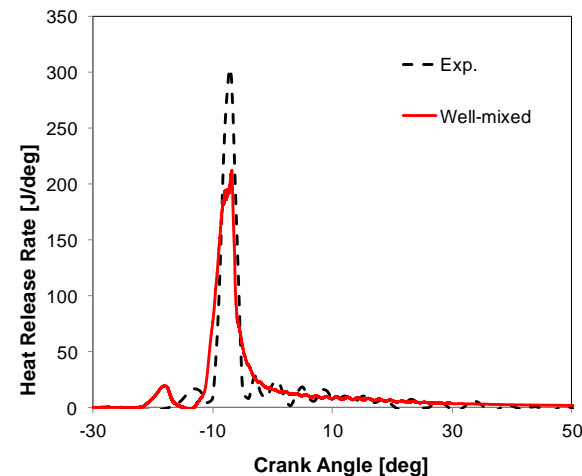
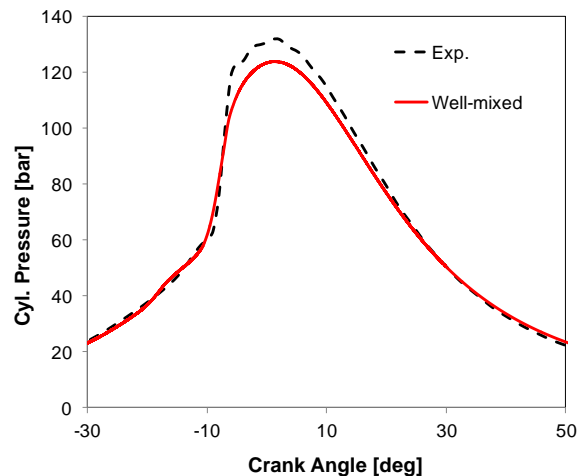
## PCCI combustion conditions

- High EGR rate (50%)
- 3000 rpm

Computational mesh  
generated automatically with  
the Polimi tool



## Combustion model: Well-mixed



Diesel fuel: n-dodecane

Kinetic mechanism: Faravelli et al. (110 species, 300 reactions)

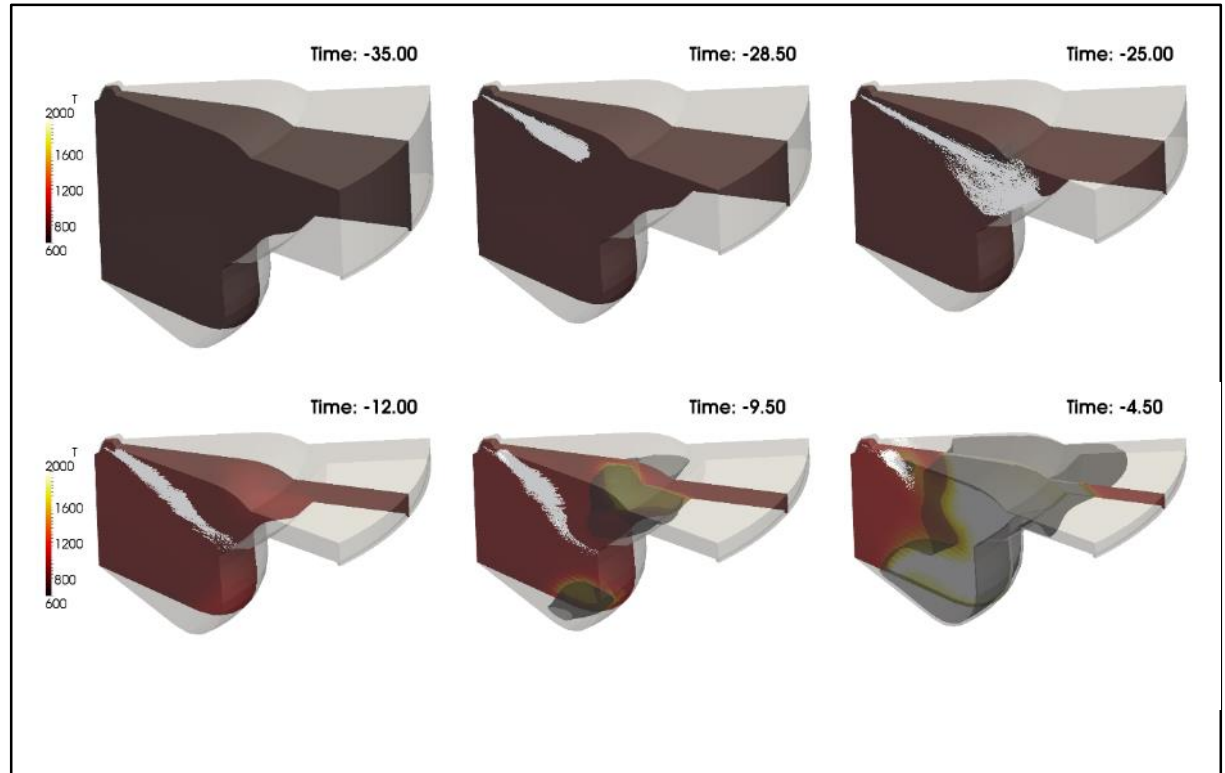
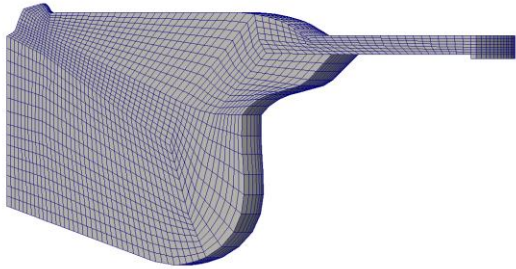
# Diesel Engines: validation

PCCI engine (support from FPT, DI Gilles Hardy)

## PCCI combustion conditions

- High EGR rate (50%)
- 3000 rpm

Computational mesh  
generated automatically with  
the Polimi tool

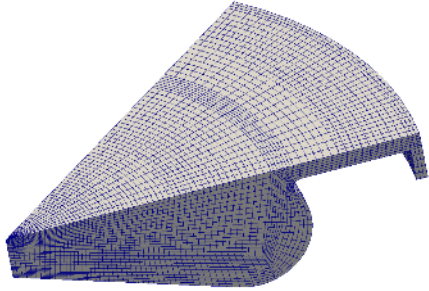




# Diesel Engines: validation

Heavy Duty engines (support from GE Global Research, Dr. Pasunurthi)

## Automatic mesh generation

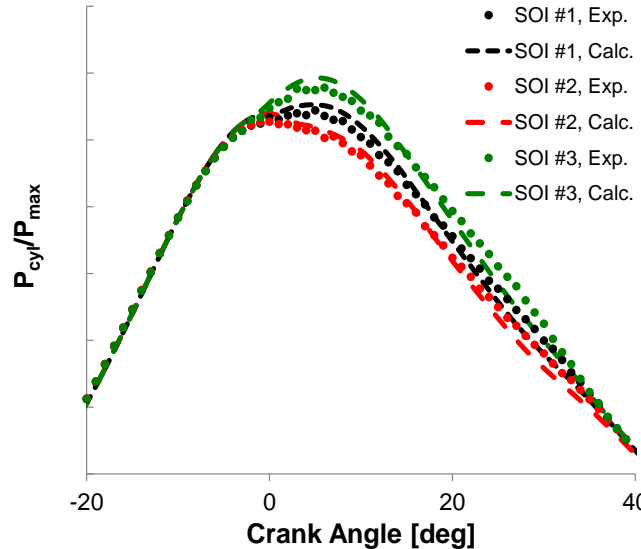


## Operating conditions

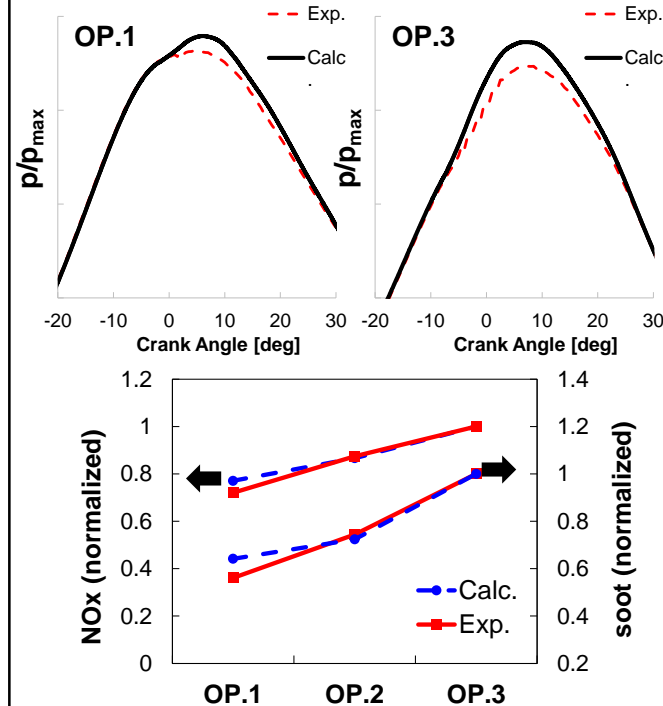
- SOI variation
- Soot/NO<sub>x</sub> trade-off
- Dual-fuel combustion
- Diesel: **mRIF**
- Dual-fuel: **PaSR**
- NO<sub>x</sub>: **Zeldovich**, soot: **Moss**

## Conventional Diesel Combustion

### Engine 1: SOI variation



## Engine 2: pollutant prediction



# Diesel Engines validation

Heavy Duty engines (support from GE Global Research, Dr. Pasunurthi)

## Setup

- Reduced mechanism for Diesel (C<sub>7</sub>H<sub>16</sub>) and natural gas
- Combustion model: PaSR

$$k = \frac{t_c}{t_c + t_{mix}} = \frac{\min \left( -\frac{\rho Y_i}{\omega_i} \Big|_{\omega_i < 0} \right)}{\min \left( -\frac{\rho Y_i}{\omega_i} \Big|_{\omega_i < 0} \right) + C_{mix} \frac{k}{\varepsilon}}$$

### Pollutants

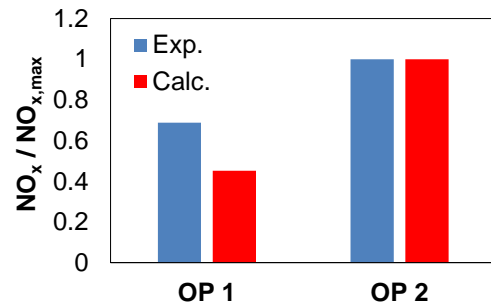
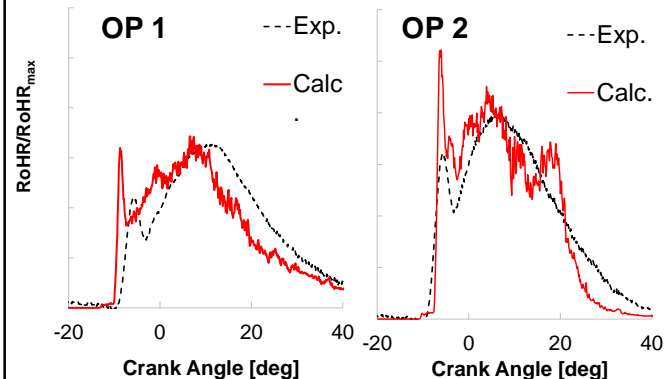
- NO<sub>x</sub> : Zeldovich
  - Soot: Moss
- Two operating points: same air/fuel ratio, different amount of injected Diesel fuel

## Dual-fuel combustion

Time: -20.00



## Validation



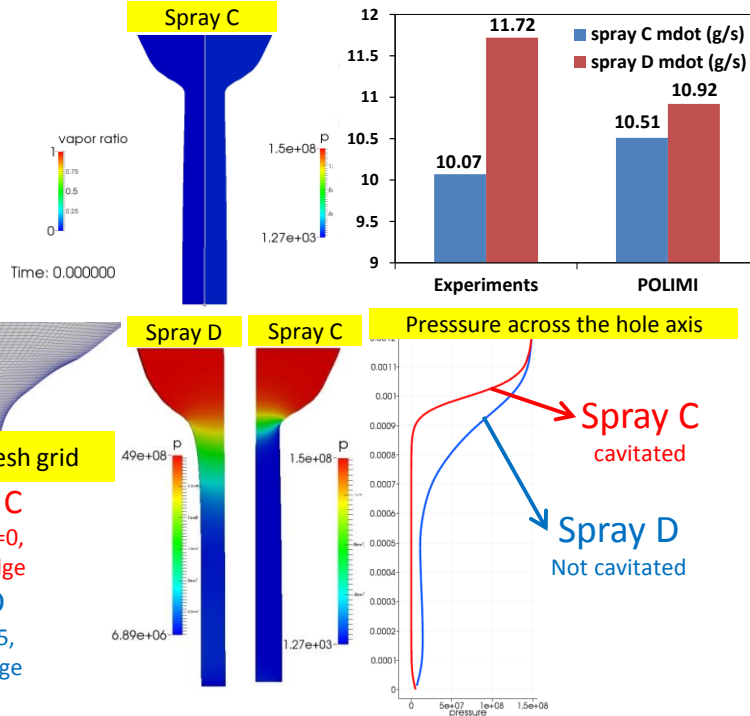
# Diesel Engines

Next steps...

## Internal nozzle flow modeling (RANS, cavitation)

### Spray C & Spray D

These two single hole injectors are defined by ECN to compare the effect of geometry on flow behavior.



## ...and more...

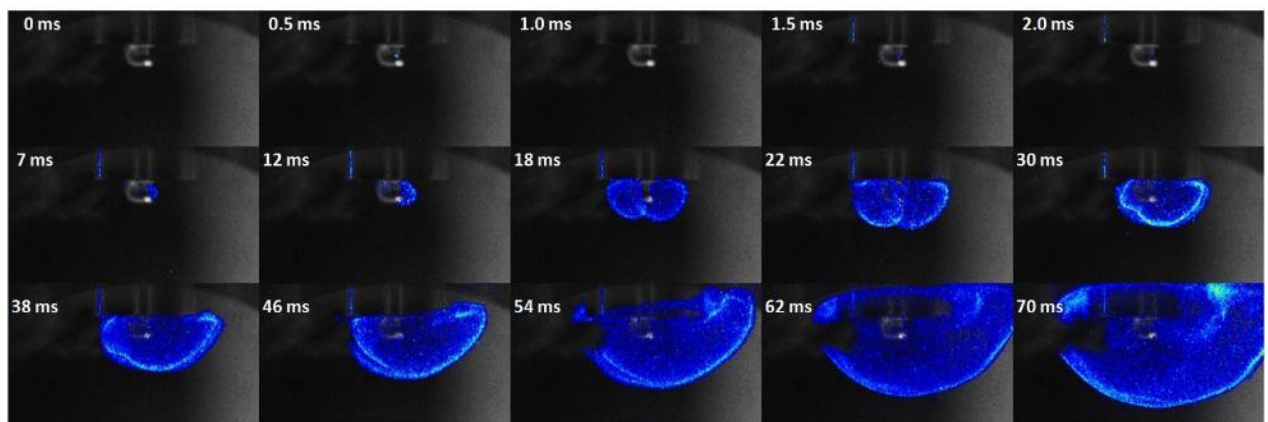
- mRIF with multiple injections

Tabulated kinetics:

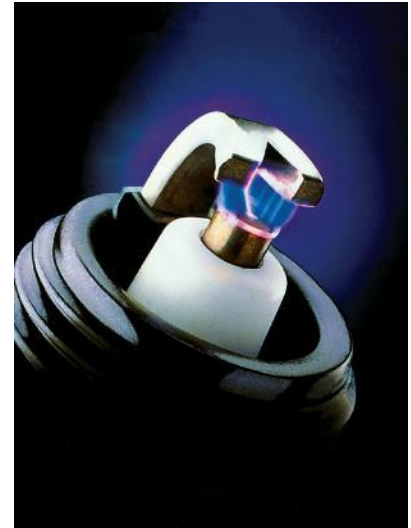
- Homogeneous reactors
- Unsteady RIF

Transported PDF combustion modeling:

- Eulerian Stochastic fields with tabulated kinetics!



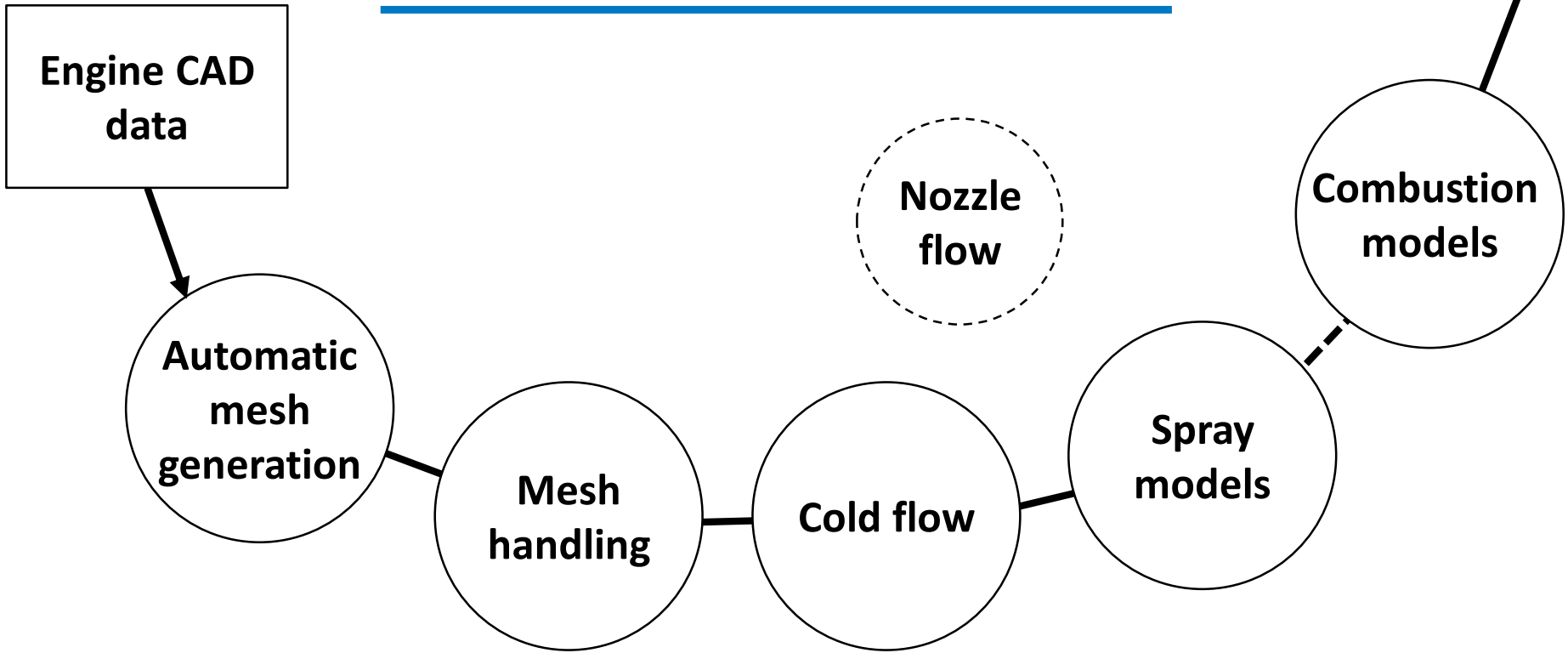
# SI Engines



# SI Engines

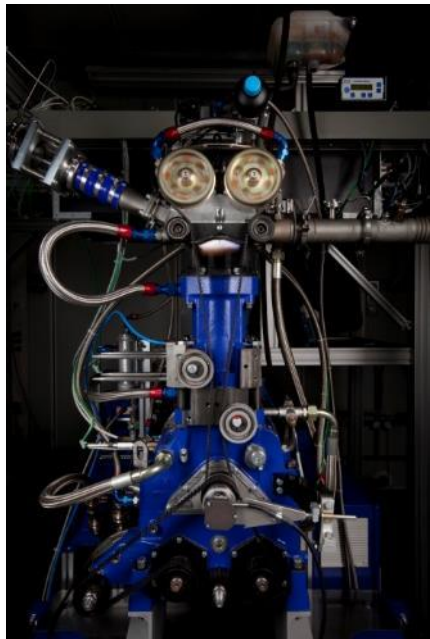
Methodology / model development

---

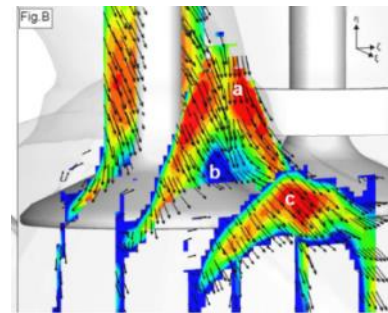
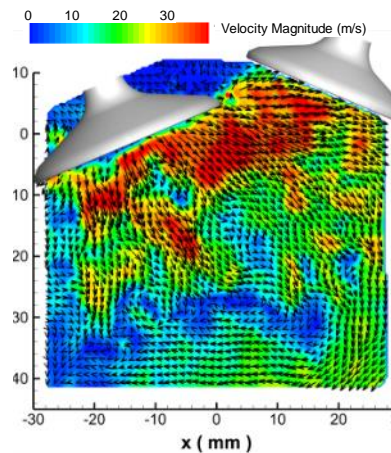
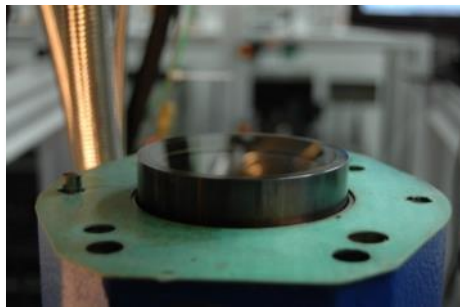


# SI Engines: cold flow

Darmstadt optical engine (collaboration with Dr. B. Bohm and DI C. P. Ding)



Four-valve engine, fully optically accessible



PIV measurement techniques:

- low repetition rate planar PIV
- high-speed PIV (HS-PIV)
- stereoscopic PIV (SPIV)
- tomographic PIV (TPIV).

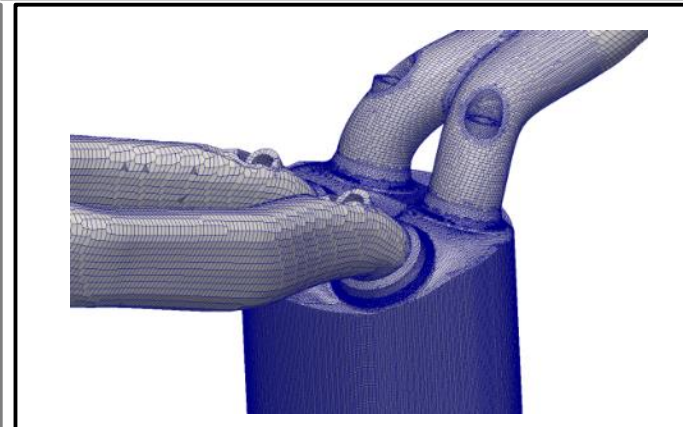
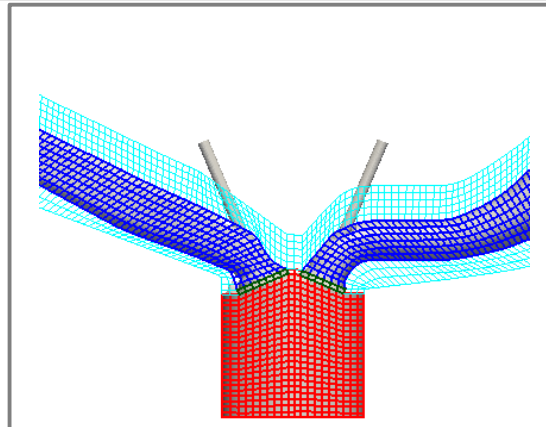
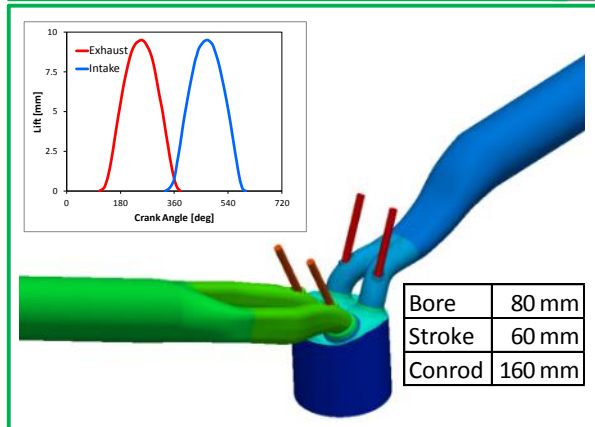
# SI Engines: cold flow

Full cycle SI: Darmstadt optical engine – automatic mesh generation

STL + data

Geometry-oriented block  
structured mesh

snappyHexMesh

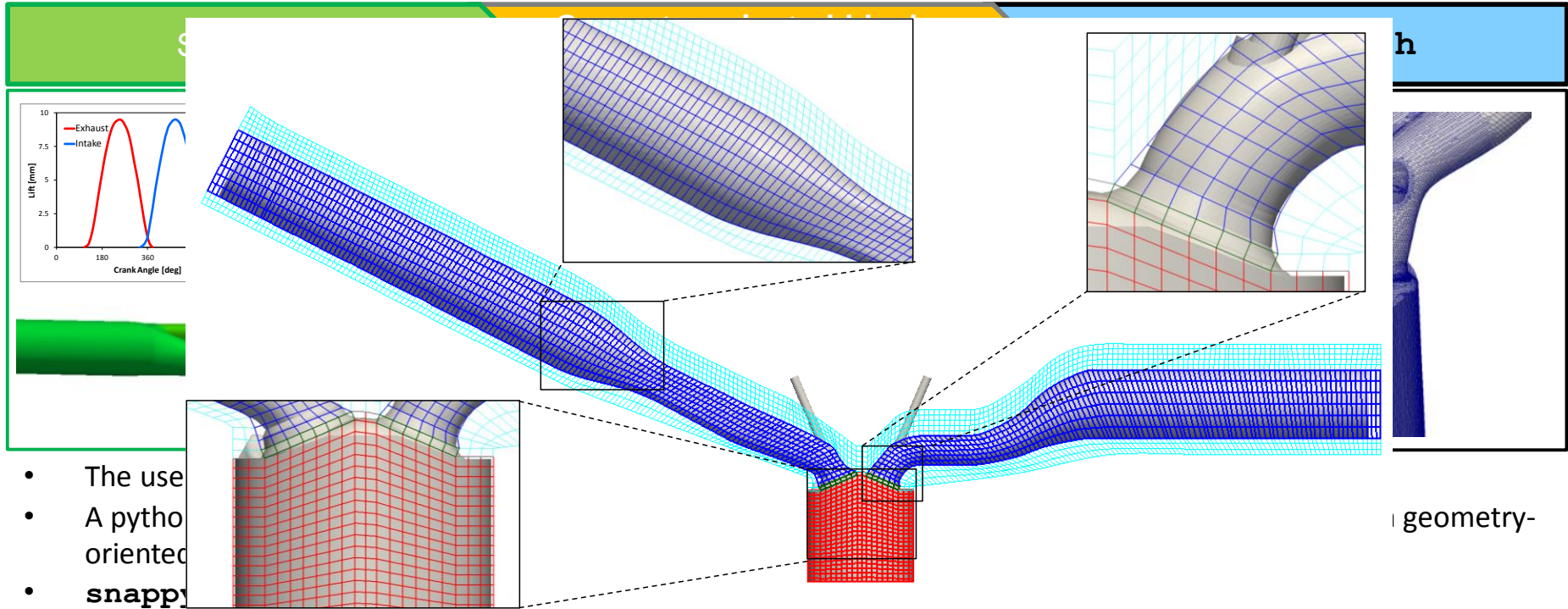


- The user provides combustion chamber geometry and data (bore, stroke, valve lifts)
- A python program automatically recognizes the direction of **ducts**, **cylinder** and **valves** and generates a geometry-oriented background grid
- **snappyHexMesh** is then run using the geometry-oriented background mesh



# SI Engines: cold flow

Full cycle SI: Darmstadt optical engine – automatic mesh generation





# SI Engines: cold flow

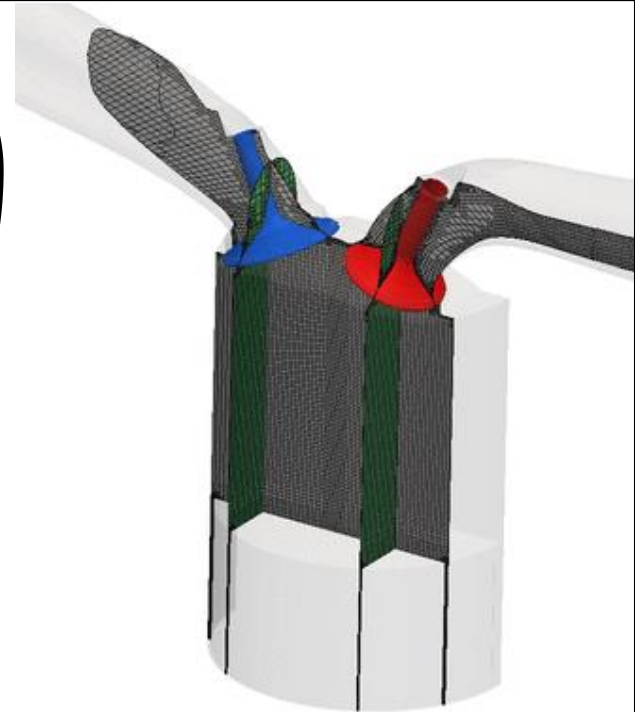
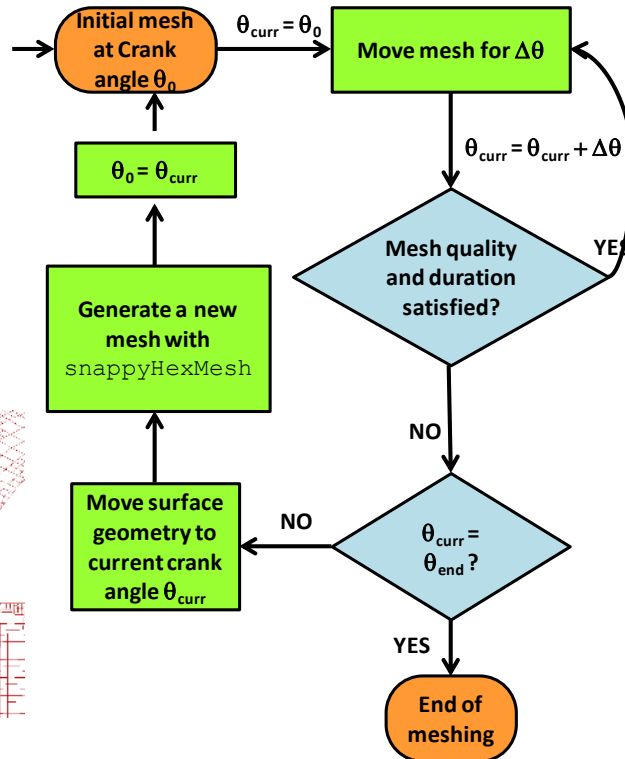
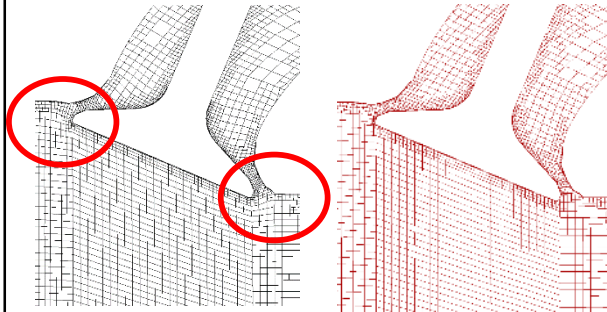
Full cycle SI: Darmstadt optical engine – mesh management

## Full-cycle simulations:

- Multiple meshes
- Mesh to mesh interpolation strategy.

## Duration of each mesh:

- User defined + quality criteria



# SI Engines: cold flow

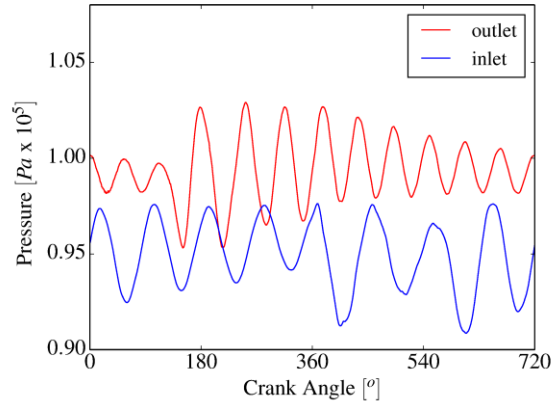
Full cycle SI: Darmstadt optical engine – case setup

## Models and boundary conditions

### Engine geometry data

Bore	86 mm
Stroke	86 mm
Compression ratio	8.5
IVO	325 CAD
IVC	485 CAD
EVO	105 CAD
EVC	345 CAD
<b>Speed</b>	<b>850 rpm</b>
Combustion	no

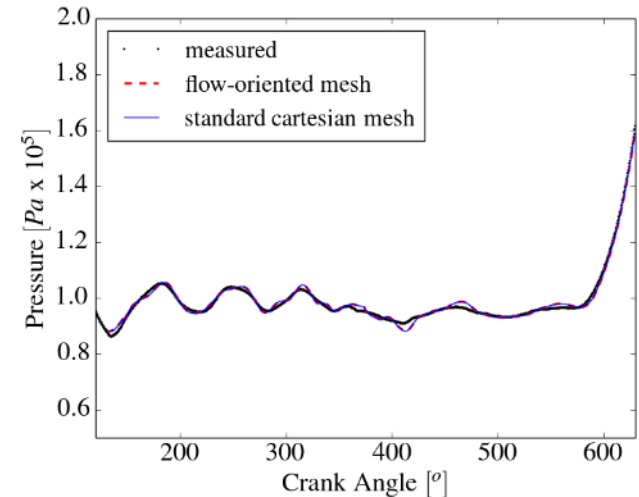
### Boundary conditions



- Unsteady boundary conditions (from exp. data) imposed at inlet and outlet ports.

### CFD models

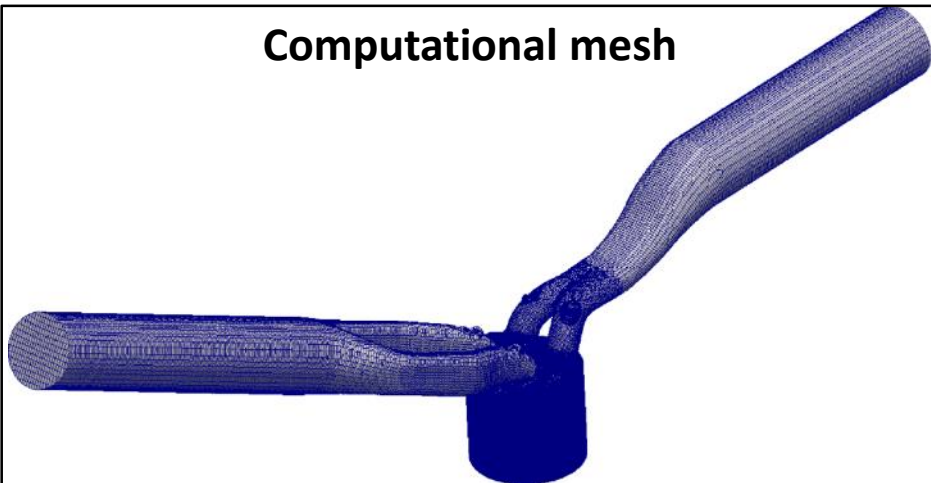
- Second-order discretization (TVD)
- Turbulence model: standard k- $\epsilon$



# SI Engines: cold flow

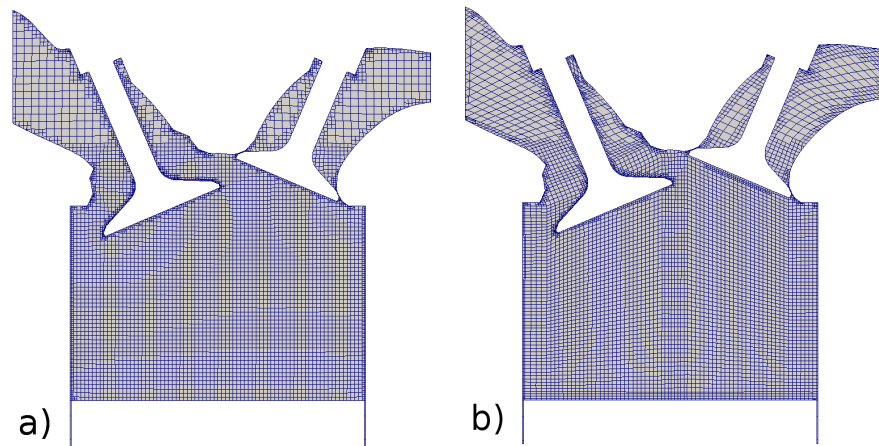
Full cycle SI: Darmstadt optical engine – case setup

## Computational mesh



- 4 mm mesh size in the ducts region;
- 2 mm mesh size in the cylinder and valve region;
- local refinement up to 1 mm close to cylinder head, piston and liner boundaries;
- local refinement up to 0.25 mm close to the valves boundaries.

## Mesh layouts

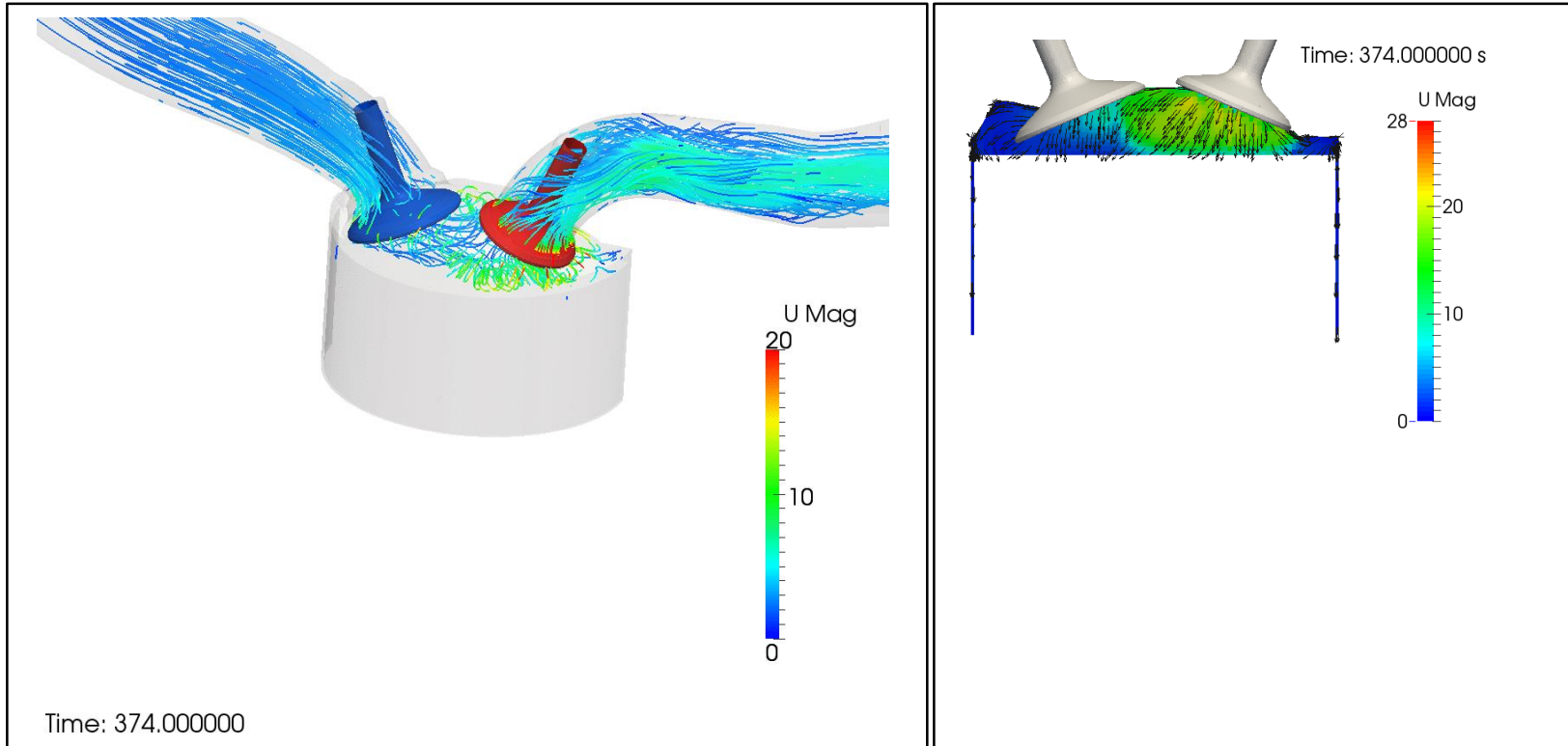


a) Cartesian mesh (automatically generated + snappyHexMesh)

b) Flow-oriented mesh (automatically generated + Polimi tool + snappyHexMesh)

# SI Engines: cold flow

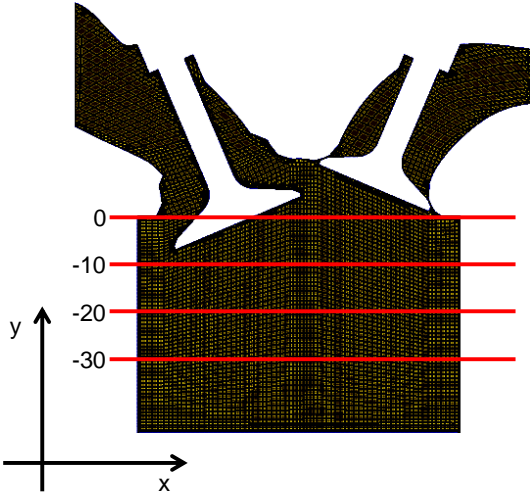
Full cycle SI: Darmstadt optical engine – validation



# SI Engines: cold flow

Full cycle SI: Darmstadt optical engine – validation

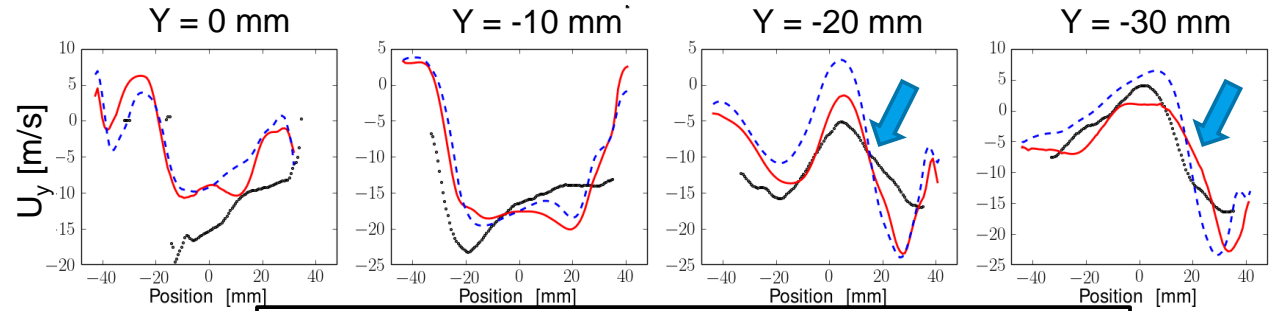
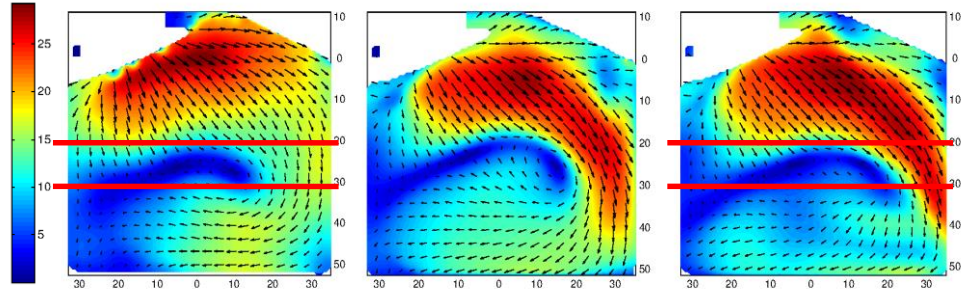
x and y velocity components along four different measurement lines located at different distances from the cylinder head.



## 450 CAD mid-intake

Similar behavior between the two grids, flow dominated by the incoming air jet

### Experimental Cartesian Flow-oriented

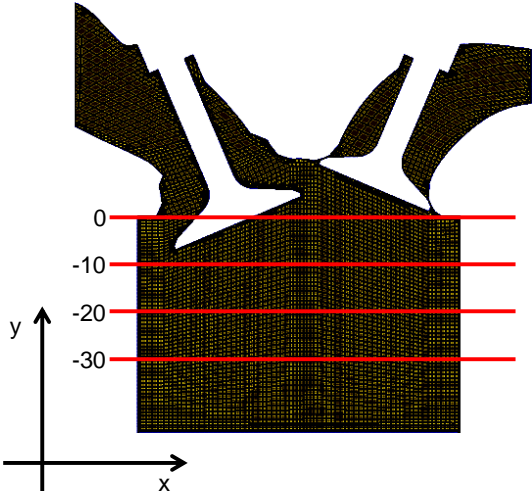


— Flow-oriented    - - Cartesian    ..... Experimental

# SI Engines: cold flow

Full cycle SI: Darmstadt optical engine – validation

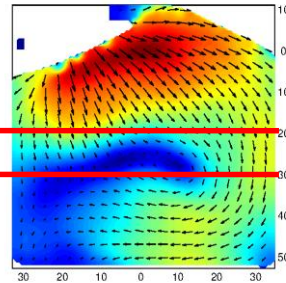
x and y velocity components along four different measurement lines located at different distances from the cylinder head.



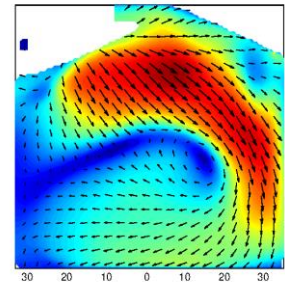
## 450 CAD mid-intake

Similar behavior between the two grids, flow dominated by the incoming air jet

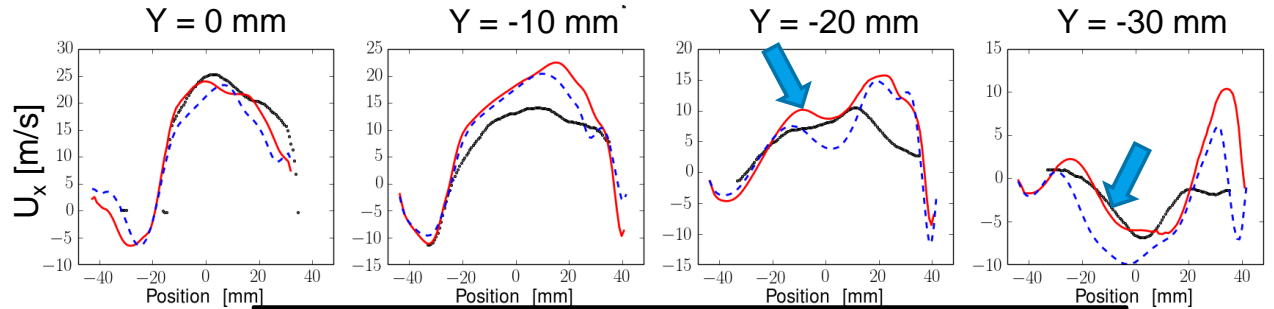
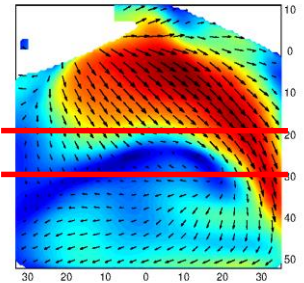
### Experimental



### Cartesian



### Flow-oriented



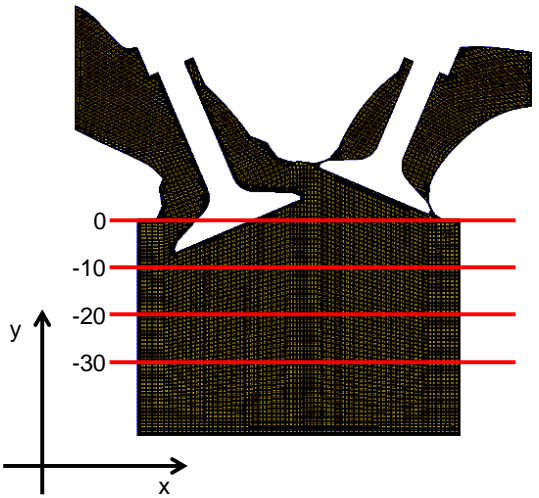
— Flow-oriented    - - Cartesian    ..... Experimental



# SI Engines: cold flow

Full cycle SI: Darmstadt optical engine – validation

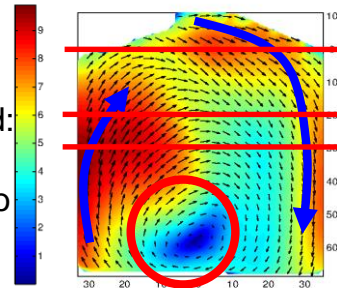
x and y velocity components along four different measurement lines located at different distances from the cylinder head.



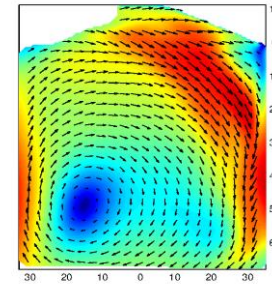
## 540 CAD BDC, intake

Better prediction of the flow oriented grid: Vortex location, distribution of the two main streams

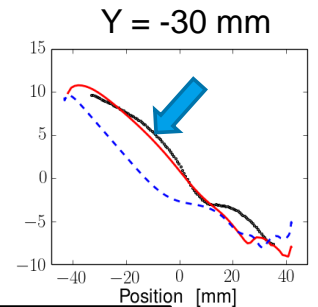
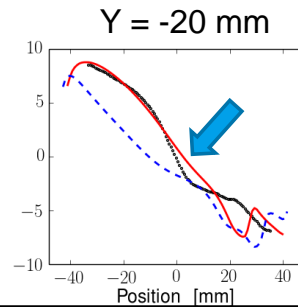
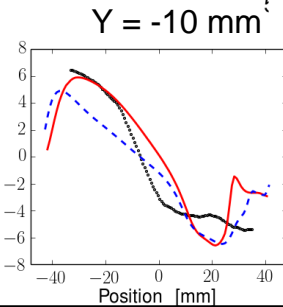
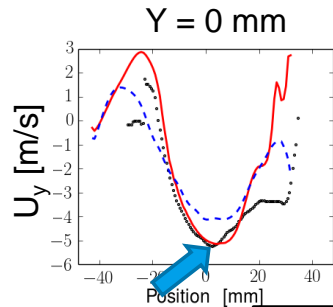
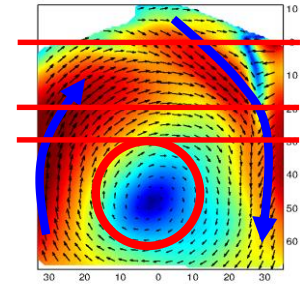
### Experimental



### Cartesian



### Flow-oriented

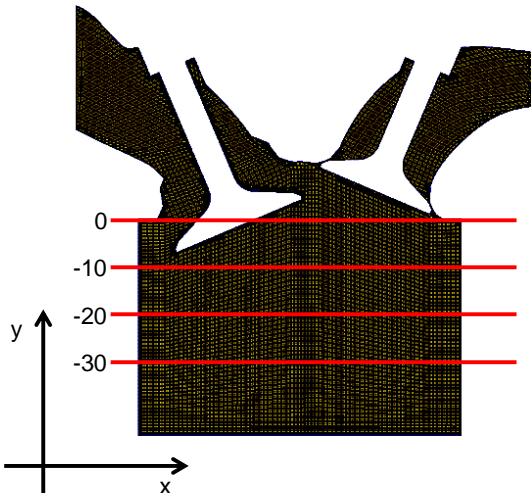


— Flow-oriented    - - Cartesian    ..... Experimental

# SI Engines: cold flow

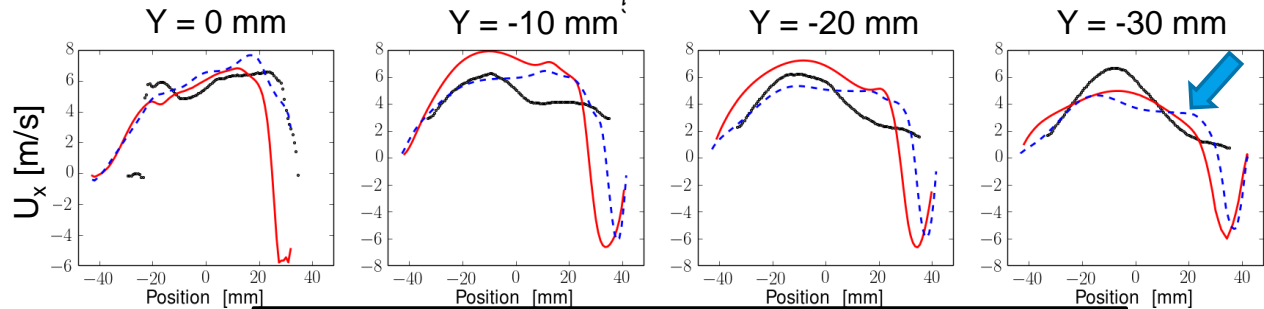
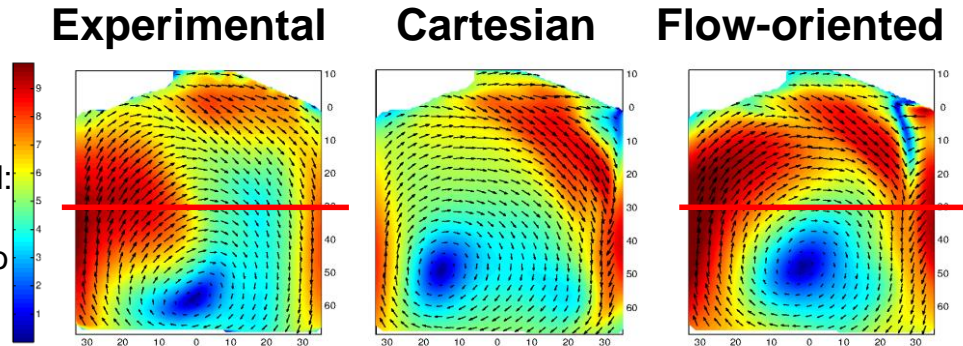
Full cycle SI: Darmstadt optical engine – validation

x and y velocity components along four different measurement lines located at different distances from the cylinder head.



**540 CAD  
BDC, intake**

Better prediction of the flow oriented grid:  
Vortex location,  
distribution of the two main streams



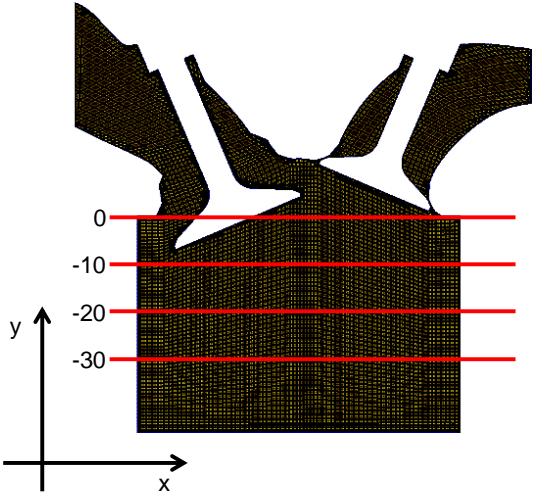
— Flow-oriented    - - - Cartesian    ..... Experimental



# SI Engines: cold flow

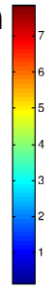
Full cycle SI: Darmstadt optical engine – validation

x and y velocity components along four different measurement lines located at different distances from the cylinder head.

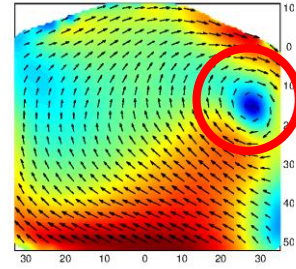


## 660 CAD mid-compression

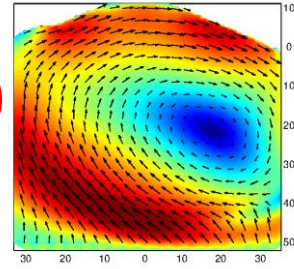
Flow-oriented grid better describe the tumble vortex structure



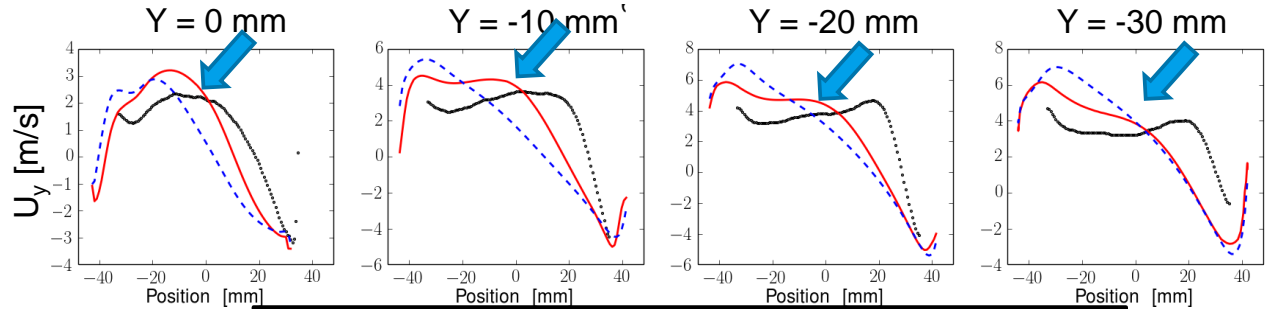
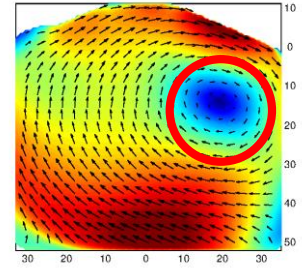
### Experimental



### Cartesian



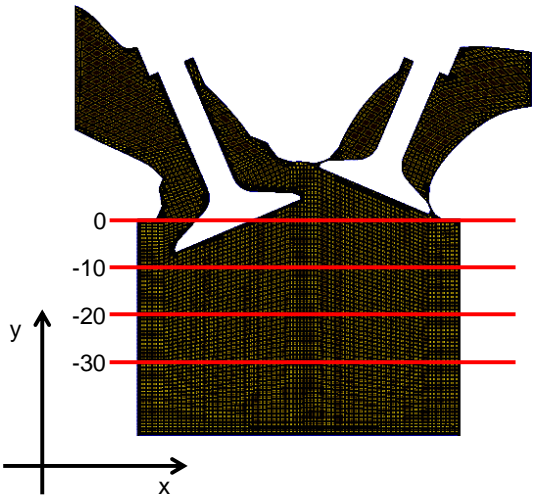
### Flow-oriented



# SI Engines: cold flow

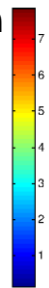
## Full cycle SI: Darmstadt optical engine – validation

x and y velocity components along four different measurement lines located at different distances from the cylinder head.

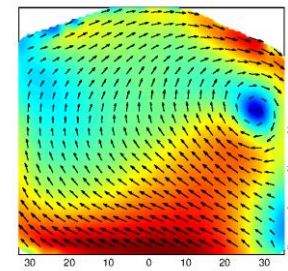


### 660 CAD mid-compression

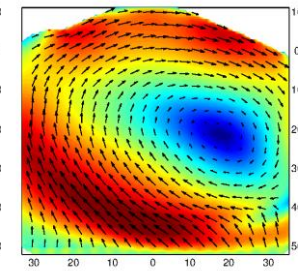
Flow-oriented grid better describe the tumble vortex structure



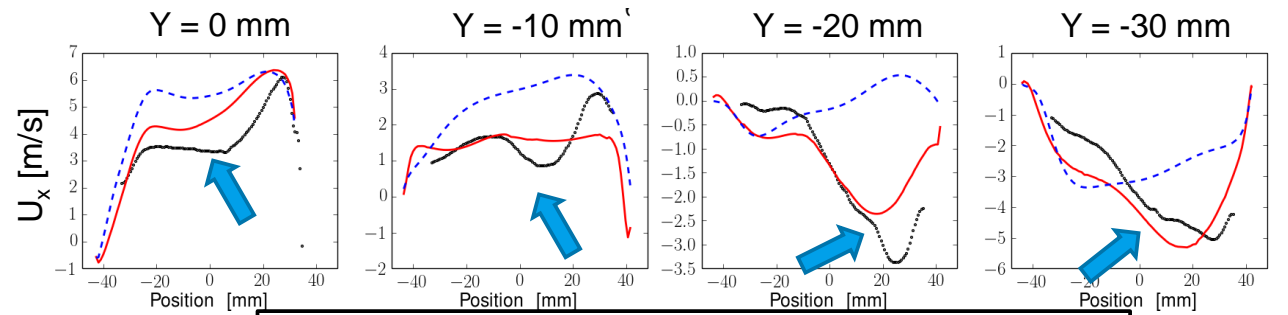
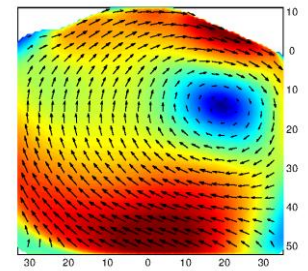
### Experimental



### Cartesian



### Flow-oriented



# SI Engines: GDI fuel-air mixing

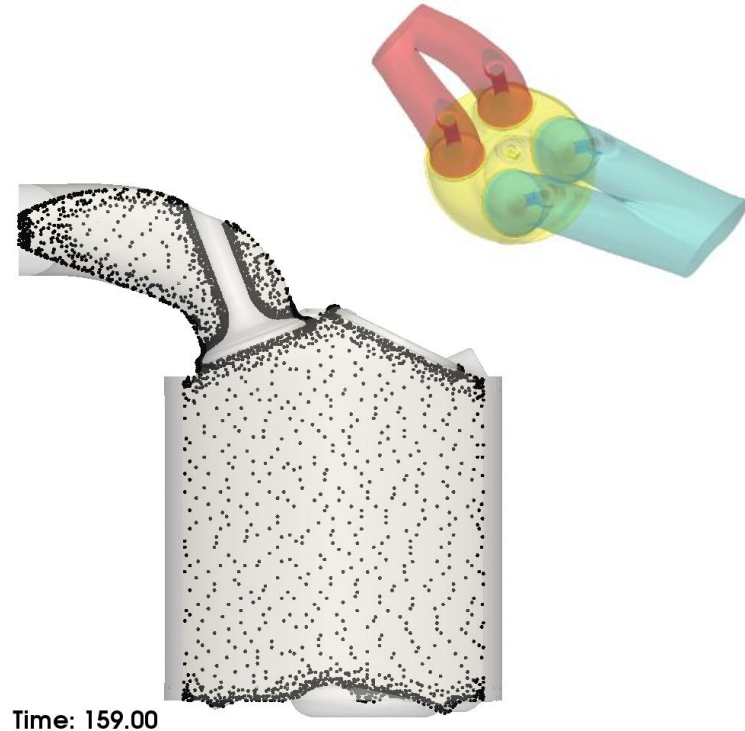
Stratified engine (collaboration with IM-CNR, Ing. Sementa, Ing. Montanaro)

## Optically accessible GDI engine

### Operating points

	Injection pressure [bar]	SOI [° BTDC]	Charge stratification
<b>1</b>	100	60	<b>High</b>
<b>2</b>	100	110	<b>Low</b>
<b>3</b>	60	60	<b>High</b>
<b>4</b>	60	120	<b>Low</b>

bmep = 7.2 bar, SA = 13 BTDC;  $\lambda = 1.15$  (lean)



# SI Engines: GDI fuel-air mixing

## Stratified engine

### Optically accessible GDI engine: optical/computed data correlation

Possible sources of soot:

- Rich pockets
- Wall-film

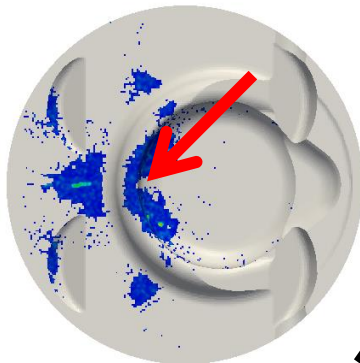
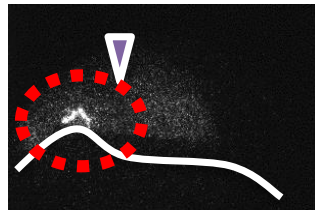
Correlated with optical soot chemiluminescence

Fuel m.f.  $P_{inj} = 100$  bar; SOI = 110 BTDC

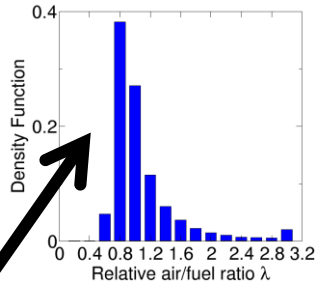
0 0.12



Soot chemiluminescence



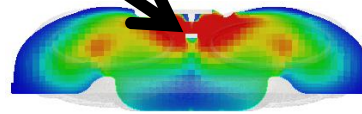
Wall-film



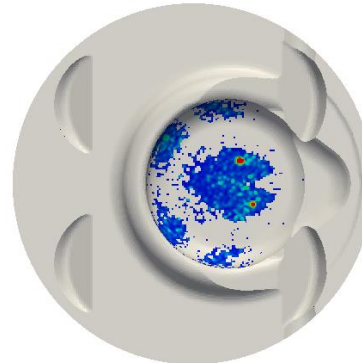
$\lambda$  distribution

Fuel m.f.  $P_{inj} = 60$  bar; SOI = 60 BTDC

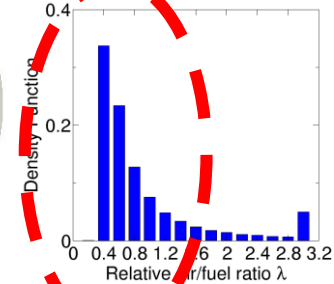
0 0.12



Soot chemiluminescence



Wall-film



$\lambda$  distribution

# SI Engines: combustion

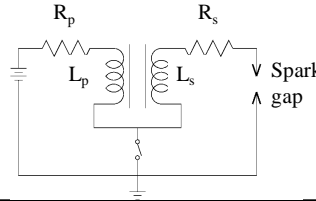
## Modeling

### Comprehensive combustion model

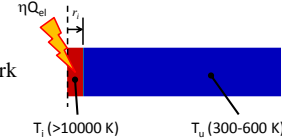
- Detailed description of the flame kernel growth process via Lagrangian approach and suitable sub-models (breakdown, electrical circuit, wrinkling)
- Coherent flamelet model for flame propagation in the Eulerian phase (gas)
- Strict coupling between Eulerian and Lagrangian phases

### Sub-models

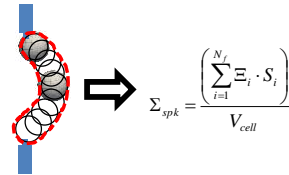
#### Secondary circuit energy transfer



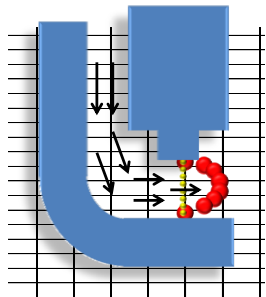
#### Breakdown



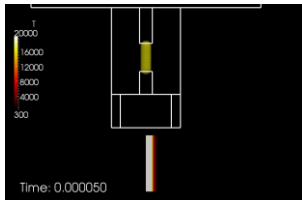
#### Flame surface density



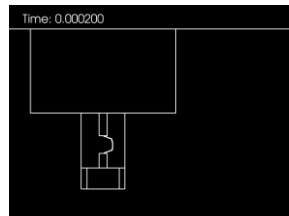
#### Lagrangian particles for the spark-channel



#### Mass and energy equations solved for the flame kernel particles



#### Particles convected by the flow, possibility to predict restrike



Time: 349.80



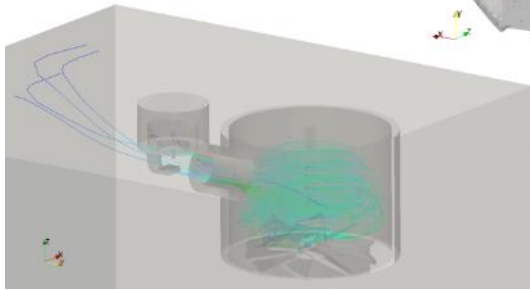
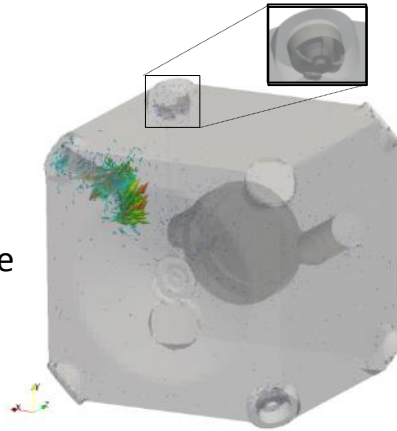
Possibility to predict the effects of local flow, mixture conditions, turbulence, electrical circuit properties (voltage, current). Prediction of misfire also possible.

# SI Engines: combustion

## Assessment and validation

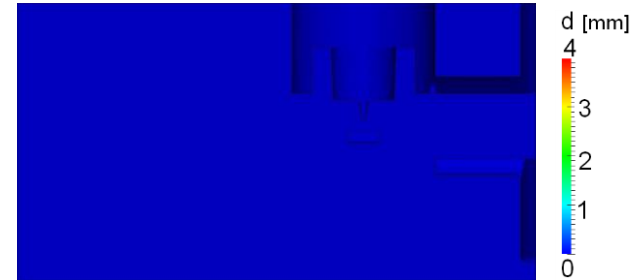
### Applications

- Pressurized vessels
- Multi-ignition systems
- Fan-generated flow velocity and turbulence fields at the spark-gap

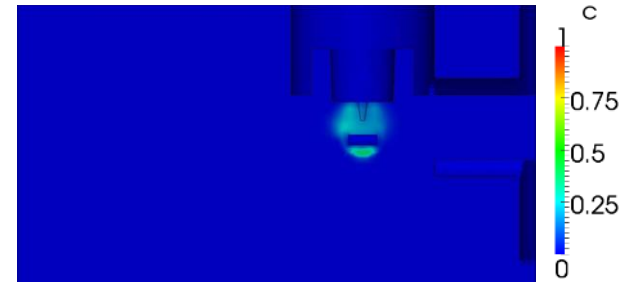


### Results

Initial combustion stage  
(Lagrangian – Eulerian coupling)



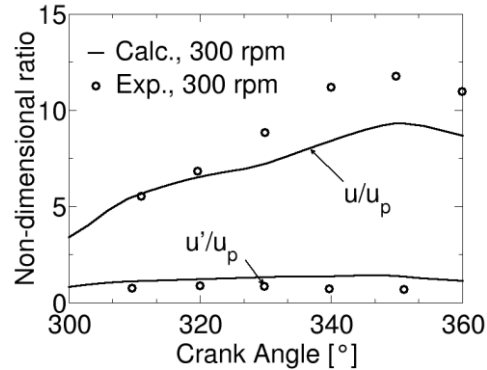
Fully turbulent flame  
(Eulerian model only)



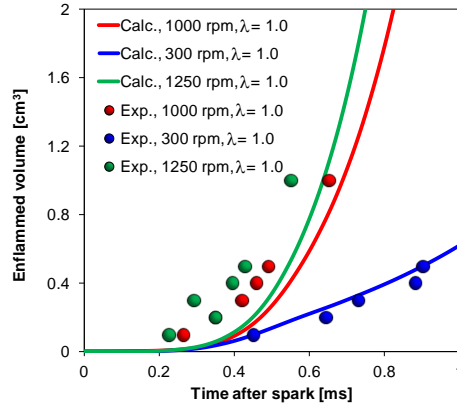
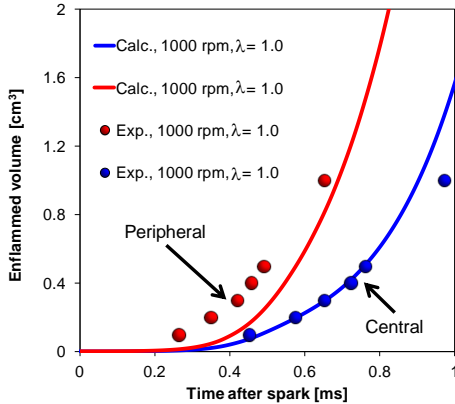
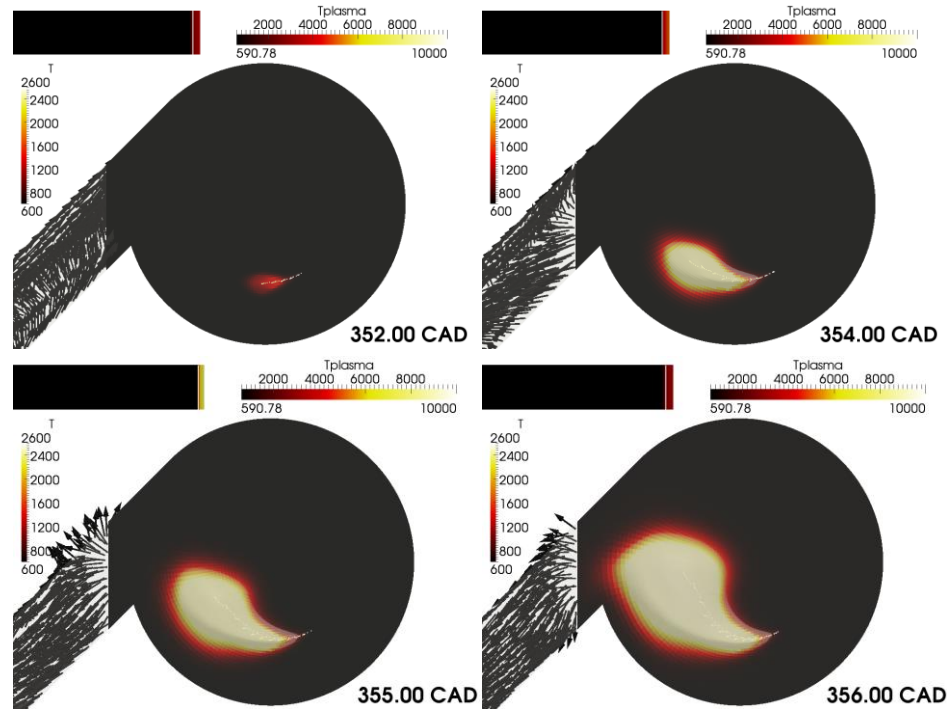


# SI Engines: combustion

## Experimental validation: Herweg and Maly Engine



### Flow field, flame propagation and plasma temperature details

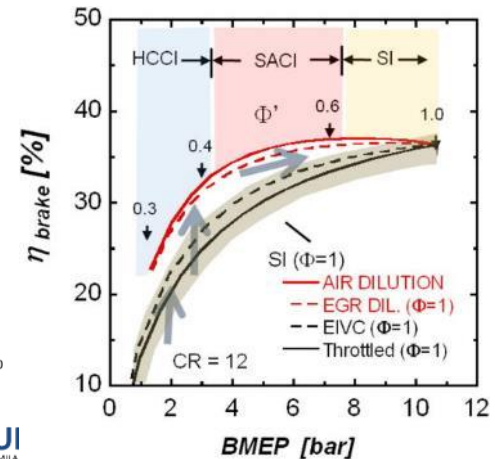
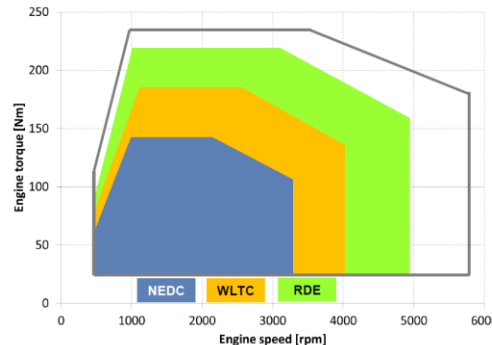




# Conclusions

## CFD modeling of in-cylinder phenomena at Polimi with OpenFOAM

- Detailed models continuously validated and improved:
  - Fundamental studies
  - Applied research
- Consolidated methodologies, currently applied in the context of industrial collaborations
- **...but there is still a lot to do!**



Thanks for your attention!

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