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Materials Science and Technology

Simulation of Heat and Mass Transfer Phenomena in Additive Manufacture Open Cell structures for Automotive Catalyst Applications

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Milano, Two-day Meeting on Simulations Using OpenFOAM Technology, 13.02.2020

Additive Manufactured catalytic converters and microwave heating for zero environmental impact



Currently, major challenges are: Cold Starts and High Exhaust Mass Flow. With contradictory requirements:

- lower catalyst thermal inertial (cold starts)
- bigger catalyst converter (high flow rate)

Further critical conditions are long low load operation, typical of hybrid powertrain systems

Focus: structures with high heat and mass transfer characteristics, as well as low flow through resistance







Catalyst performance under mass transfer limitation (steady state)

Simulations for geometrical optimization: CH_4 oxidation in air is studied



 Infinite fast Chemistry, mass transfer limited regime —> Steady state
____ reactingSimpleFoam

Single Region No CHT (<3°C),
T_{in}=700 K T_w=750 K

- Homogeneous reaction non considered,
- Heterogeneous reactions modelled as B.C.

Oxidation of methane

 $X_{sCH4}=0$

Other species : $\frac{\partial X_i}{\partial n} = \alpha_i \frac{M_i}{M_{CH4}} \frac{\partial X_{CH4}}{\partial n}$

Inert specie: N₂

- 4x2x2 Cells + periodic B.C
- Wash coat not modelled



Standard Mesh with increasing resolution towards Empa the surface



- 1. Cartesian Block Mesh
- 2. Foam Surface (STL file)
- 3. Castellate Mesh
- 4. Snapp to surface
- 5. Add Layer



Sample Cubic 45 Cells results:





Inert Specie: N₂

Optimization of cell geometry





1. Rotated cubic cell is the optimal cell for a lattice structure, higher K and I at all velocities





At vel=10m/s C45 requires 4 times less S_w than HC, but 3/2 bigger Volume ($S_{VHC} = 6S_{WCUBIC45}$) Performance index, I, according to Groppi: $\Delta P \cdot \rho \cdot U$

2. Rotated cubic cell is the optimal cell for a lattice tempa structure at all ϵ ,

Higher ε means lower K, but higher I

ε (0.8-0.95), same d_s



3. Lower ds means higher K and higher I



ε (0.8-0.95), ds (0.5-1) mm,

Mass Transfer





conversion/pressure drop trade

$$K = -\frac{\ln(1-\eta)}{S_v V/Q_{in}}$$
$$S_w = S_v V \propto 1/K$$

BEST: Cubic45, higher ε, lower d_s

Manufacturing, canning and testing of real size polyhedral catalyst substrates





 Manufacturing and stability constraints: restrict possible parameters

 $\epsilon \le 0.9$ d_s ≥ 1 mm









- Hybrid method: AM of the stamp, REPLICA method for the substrates
 - Ls = 3.9 mm $d_s = 1.2 \text{ mm}$ $\epsilon = 0.8$ Sv= 743 m²/m³

We have succeeded in almost reaching the benchmark, the over years developed product has

still superior performances **REF HC** HC AM 1/5PGM V, V. Ref.Ka 1/5 Sw, Sw, V, 3dKat PGM 1/5 PGM Sw, Vergle 1/5PGM -15 % -1% -5 % 100% 100% 100% 90% 90% 90% 80% 80% 80% 70% 70% 70% 60% 60% 60% 50% 50% 50% Bag 1 Bag 2 Bag 3 Total Bag 1 Bag 2 Bag 3 Total Bag 1 Bag 2 Bag 3 Total

T.HC [%]

NOx [%]

CO [%]

AM have lower pressure loss







Manufactured Cordierite 3D catalysts had a higher strut diameter than anticipated





$$\varepsilon = \frac{V_o}{V_{TOTAL}}$$

$$S_V = \frac{S_W}{V_{TOTAL}}$$



Comparison of entire catalysts with identical V: cubic45 higher conversion than HCs with 2 time less surface





For the simulated configurations, no evident disadvantages in pressure drop







Catalyst performance in transient cold starts

OpenFOAM full-scale, multi region, converter SIMULATIONS: CO oxidation in DOC



From micro scale simulations or

experimental correlations: Coupled SOLID-FLUID Geometry model Permeability model Heat transfer models Mass transfer model ٠ **Reaction models** SOLID **Bulk gas model** AM strucutre **Gas reactions** mid position heat mass Near wall gas model Washcoat model heat Substrate model **FLUID Surface reactions**

Case study: exhaust inflow mF=const with $TF_{in}(x=0,t)=const > TS(t=0) 373K < TF_{in}(x=0,t) < 410K$ 260K < TS(t=0) < 360K



In the entrance, solid is heated up, downstream the fluid is cooled down

 TF_{in} =425K TS(t=0s)=260K m_F=0.0172kg/s

Heat convected is highest in the upstream, however the duration of the heat exchange increases in the downstream: almost homogeneous energy exchange

$$l_{\text{conv,i,t}} = \frac{\dot{m}_{F}c_{PF}}{\Delta V} (T_{F,i,t} - T_{F,i+1,t})$$

Introduction of dimensionless time, space and temperature differences

$$\theta_{S} = \frac{T_{S} - T_{0}}{T_{F,in} - T_{0}} \qquad \theta_{F} = \frac{T_{F} - T_{0}}{T_{F,in} - T_{0}} \qquad \xi = \frac{4Nu\lambda_{F}x}{\dot{m}_{F}c_{PF}} = NTU_{\theta} \qquad \tau = \frac{4Nu\lambda_{F}t}{A_{S,FRONT}\rho_{S}c_{S}}$$

$\theta_{\rm F}$ is neither a function of $T_{\rm S}(t=0)$ nor $T_{\rm Fin}$, $\theta_{\rm F}$ is a function of length and $m_{\rm F}$

Heat up can be described as an exponential function of τ/ξ

Numerical Simulations lead to new catalyst structures in combination with new manufacturing techniques

- Worldwide first AM manufactured catalyst converter has been tested on a vehicle (manufacturing, coating, mechanical stability, integration)
- Conversion characteristic with 1/5 of precious metals is good almost on the level of the benchmark HC
- Flow resistance lower than benchmark HC
- Experiments confirmed simulation results

Understanding the heat up inside the catalyst is important for cold start reduction

- In the entrance, solid is heated up, downstream the fluid is cooled down
- The introduction of dimensionless temperature differences, time and space evidences the self similarity of the catalyst heat up before reactions start
- The catalyst heat up can be approximated analytically with a double logarithmic function in dimensionless coordinates
- Evaluation and assessment of preheating strategies

Thank You!

Questions?