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# Towards a Euler-Euler multi-fluid solver for dense spray applications

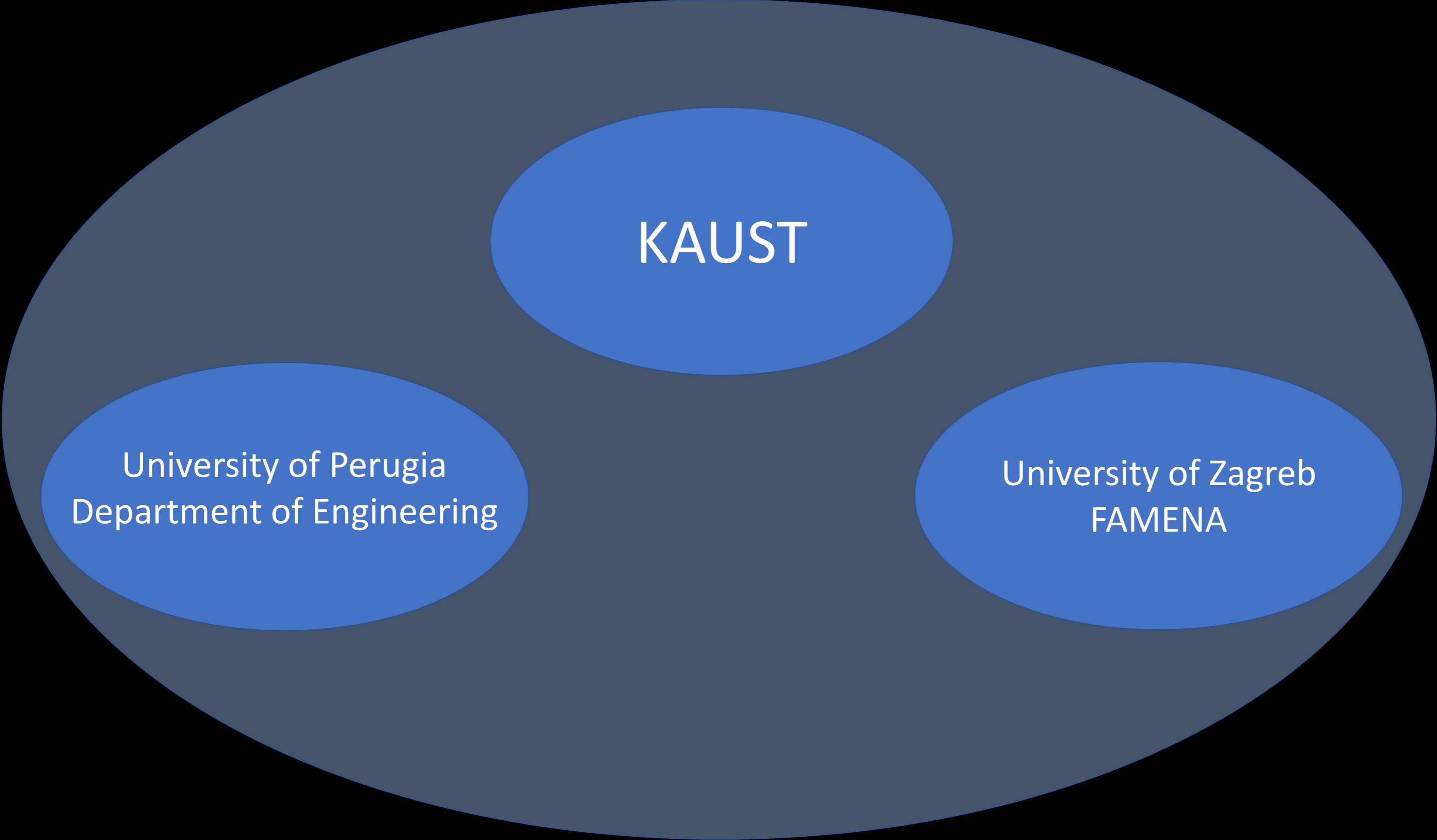
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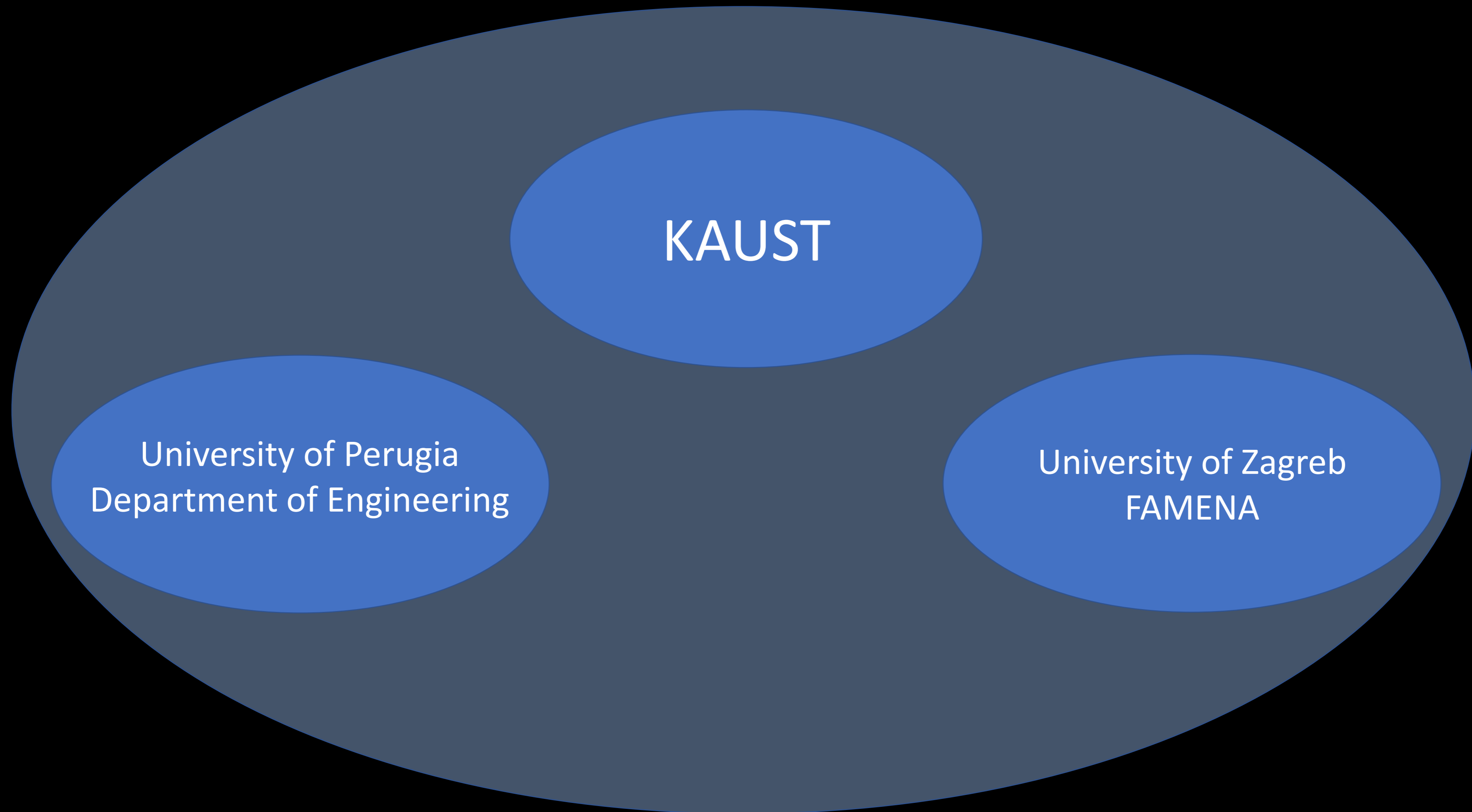
**Robert Keser**, Hrvoje Jasak, University of Zagreb

Michele Battistoni, University of Perugia

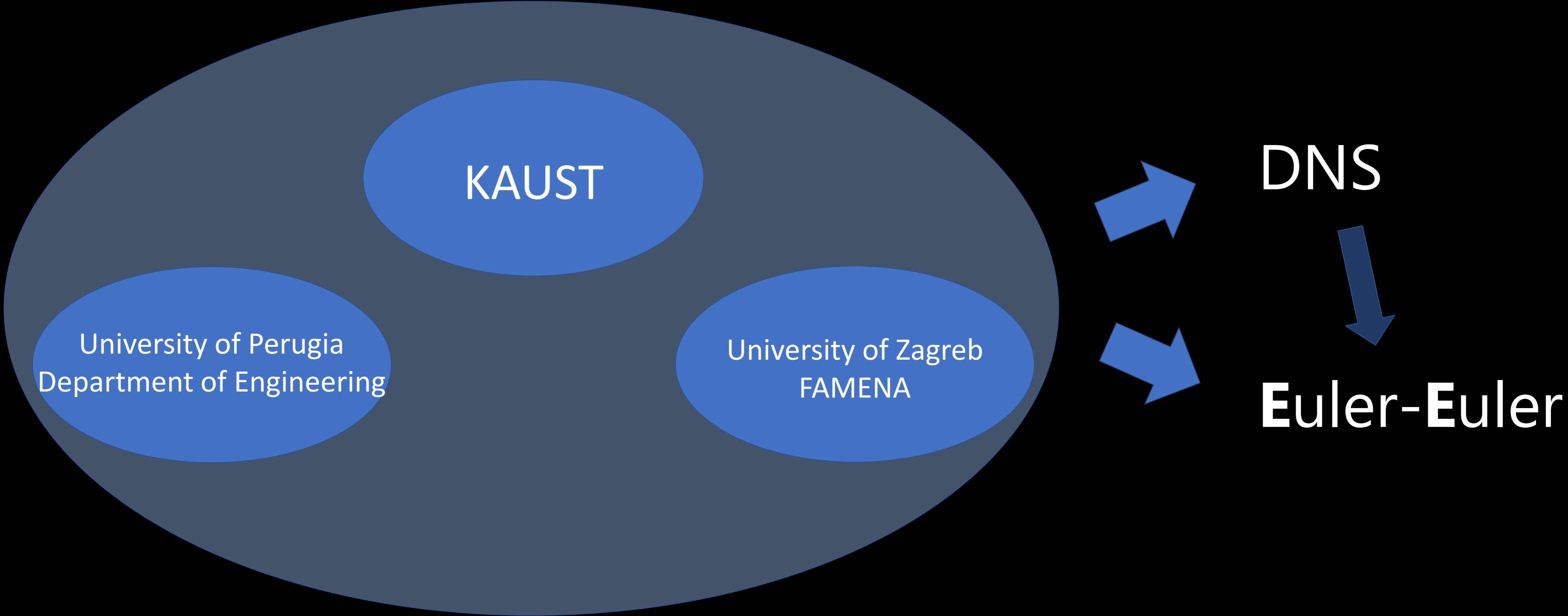
Alberto Ceschin, Hong G. Im, King Abdullah University of Science and Technology

# Predictive Modelling and Experimental Validation of Multi-component Dense Spray Dynamics





develop and establish high-fidelity modelling and experimental capabilities to predict and characterize multi-component dense fuel sprays



# Main parts of the presentation

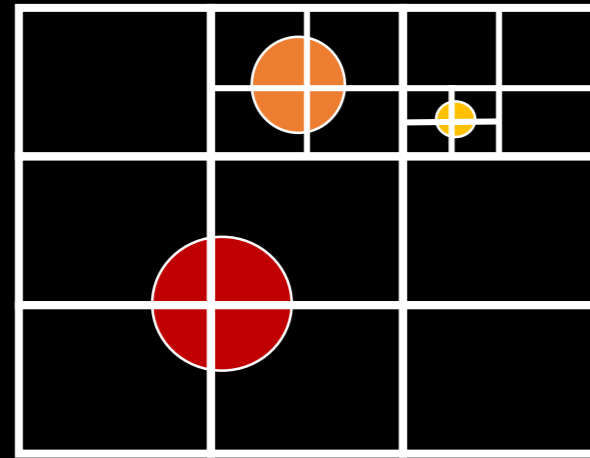
## 1. DNS solver

- Solver description
- Preliminary results

## 2. Euler-Euler solver

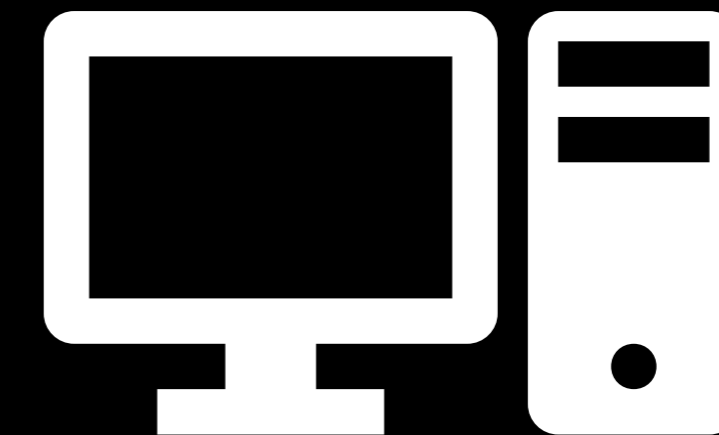
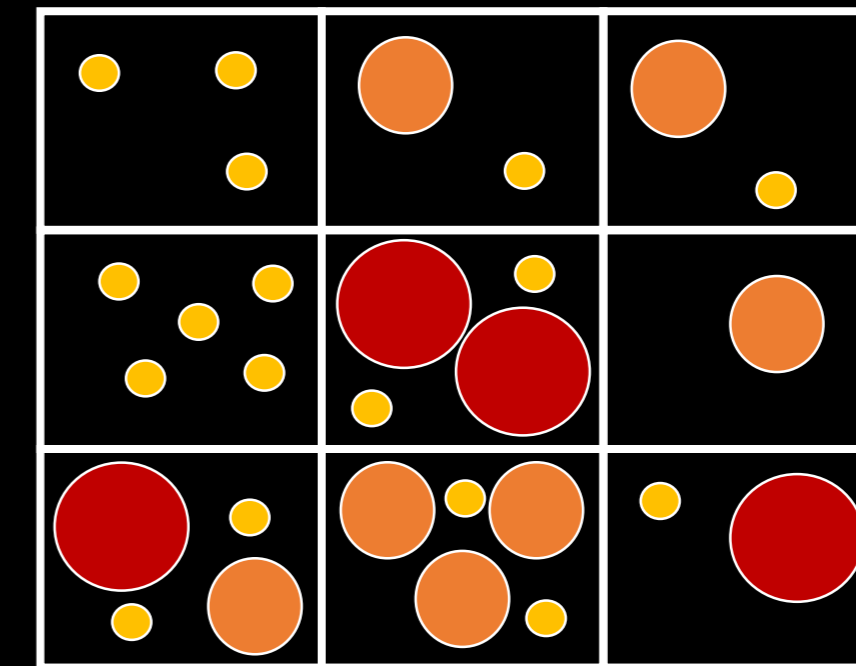
- Solver description
- Sub-model validation
- Preliminary spray simulations

# DNS



None

# E-E

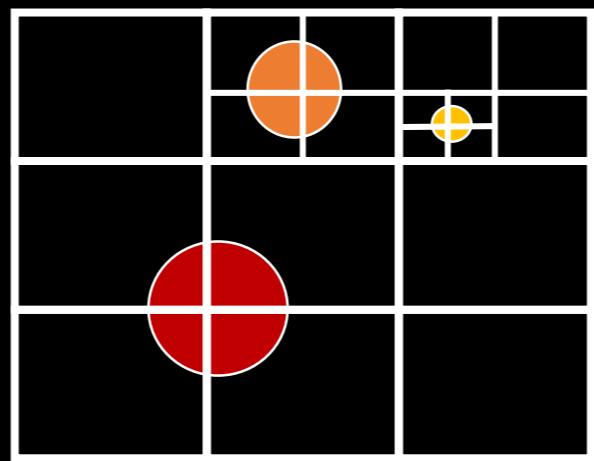


$$\begin{aligned} \overline{M}_{d,i} = & \alpha_{d,i} C_{d,i} \frac{3\overline{\rho}_c}{4d_i} |\overline{U}_{r,i}| \overline{U}_{r,i} && \text{drag} \\ & + \alpha_{d,i} C_l \overline{\rho}_c \overline{U}_{r,i} \times (\nabla \times \overline{U}_c) && \text{lift} \\ & + \alpha_{d,i} C_{vm} \overline{\rho}_c \left( \frac{D_c \overline{U}_c}{Dt} - \frac{D_{d,i} \overline{U}_{d,i}}{Dt} \right) && \text{virtual mass} \\ & - C_{d,i} \frac{3\overline{\rho}_c \nu_c^t}{4d_i \sigma_\alpha} |\overline{U}_{r,i}| \nabla \alpha_{d,i} && \text{turbulent drag} \end{aligned}$$

$$C_{d,i} = C_{d0,i} (\exp(3.64 \alpha_{d,i}) + \alpha_{d,i}^{0.864})$$

where

$$C_{d0,i} = \exp(-51.8 + 13.2 \ln(\text{Re}_i) - 0.824 (\ln(\text{Re}_i))^2)$$



**DNS**

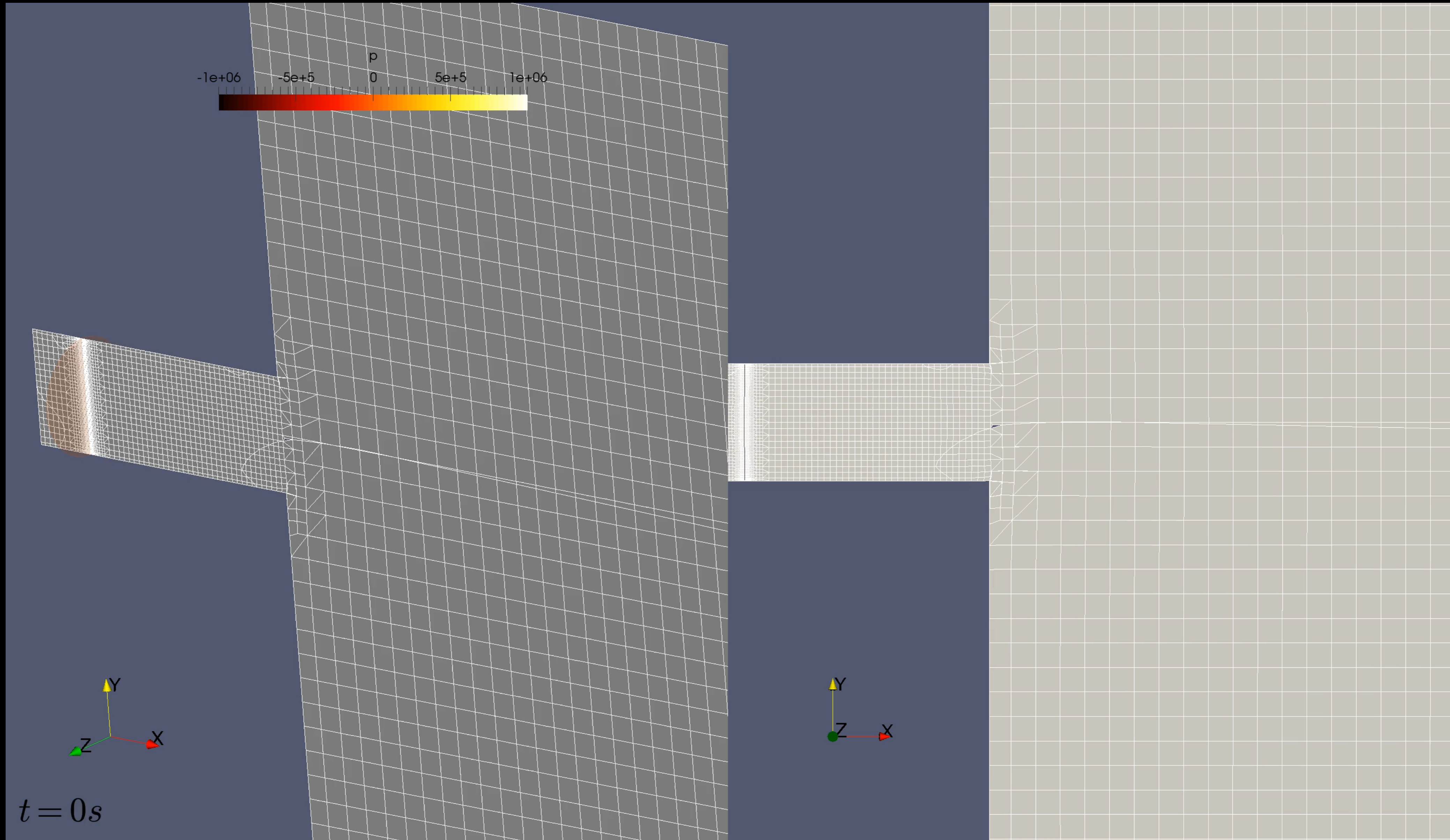


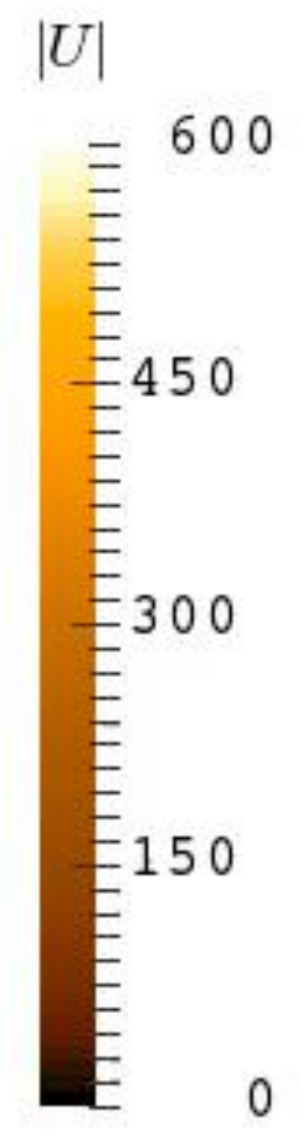
# DNS solver

- Incompressible two-phase flow (fuel and air)
- Discontinuity at the interface due to the density jump and surface tension effects taken into account with the Ghost Fluid Method
- Geometric Volume-of-Fluid method used to represent and reconstruct the sharp interface
- Adaptive Grid Refinement with Dynamic Load Balancing



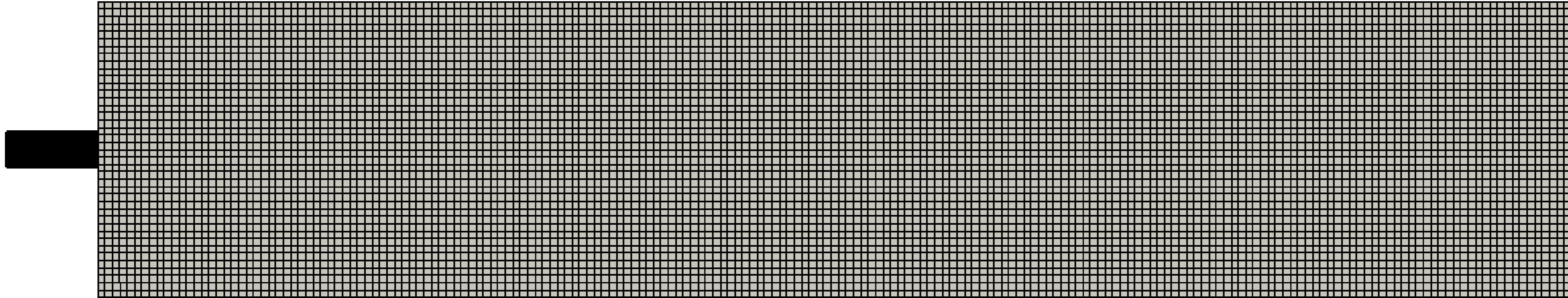
```
Perform AGR
if AGR performed and  $N_{min}/N_{max} < \Delta$  then
    Perform DLB
end if
Solve pressure correction equation
while  $i_{SIMPLE} < N_{SIMPLE}$  do
    Solve momentum equation
    while  $i_{PISO} < N_{PISO}$  do
        Solve pressure equation
    end while
    Advect interface
    Assemble GFM discretisation data
end while
```



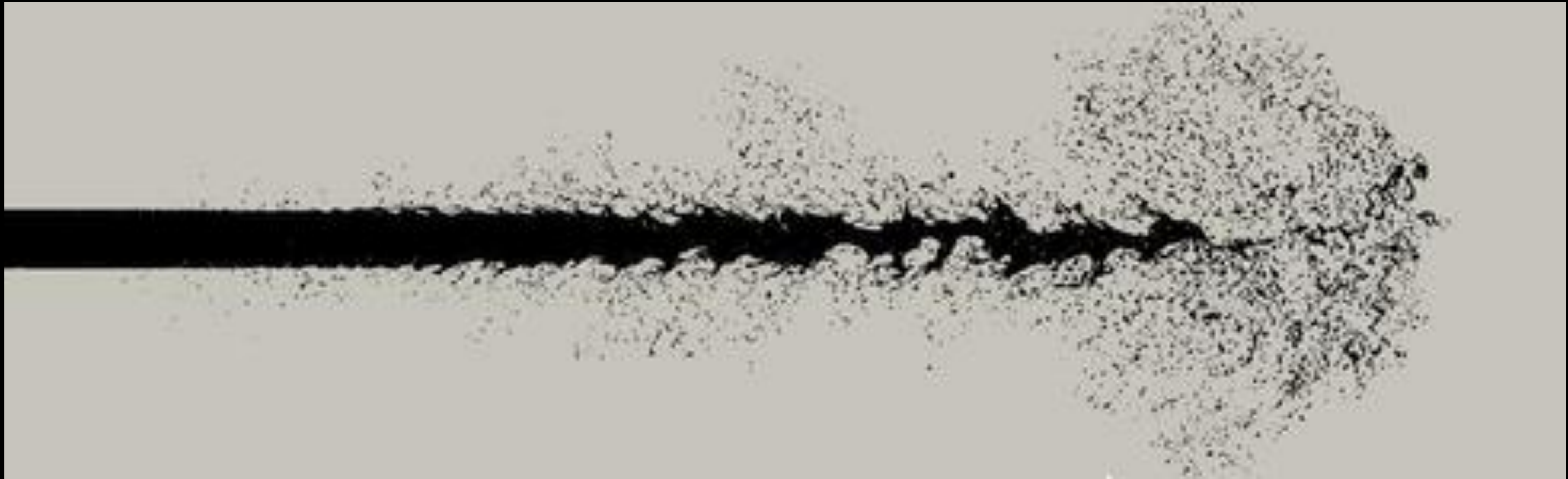
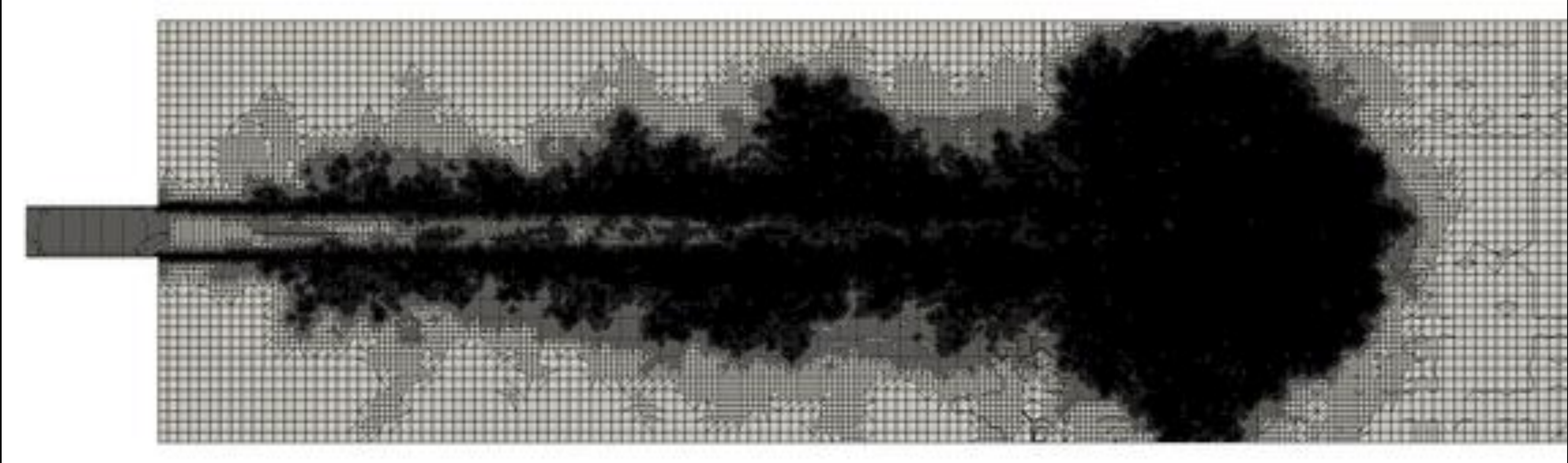


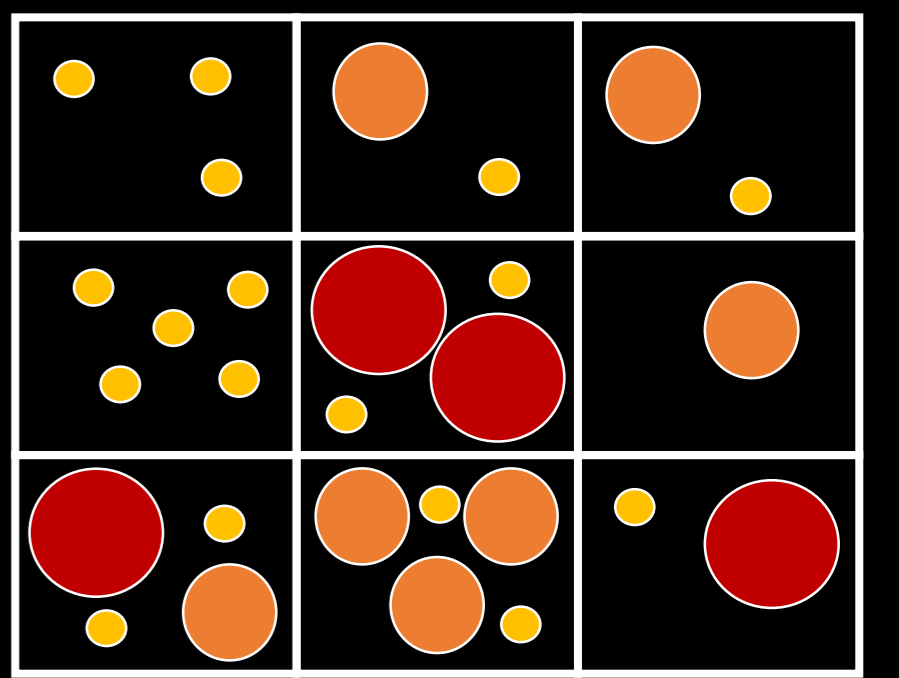
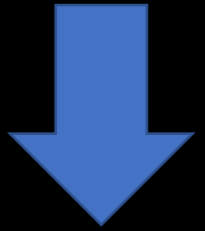
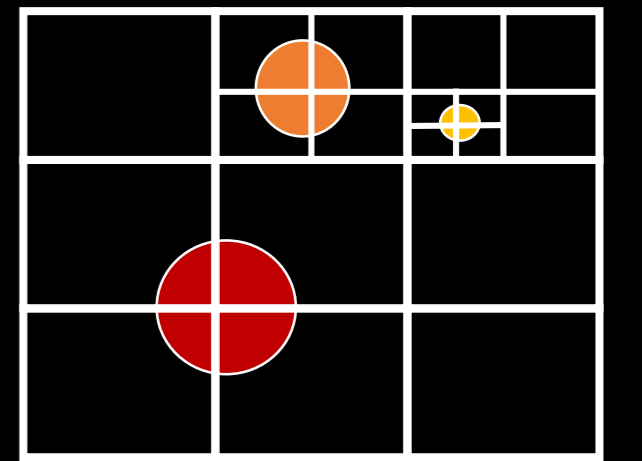
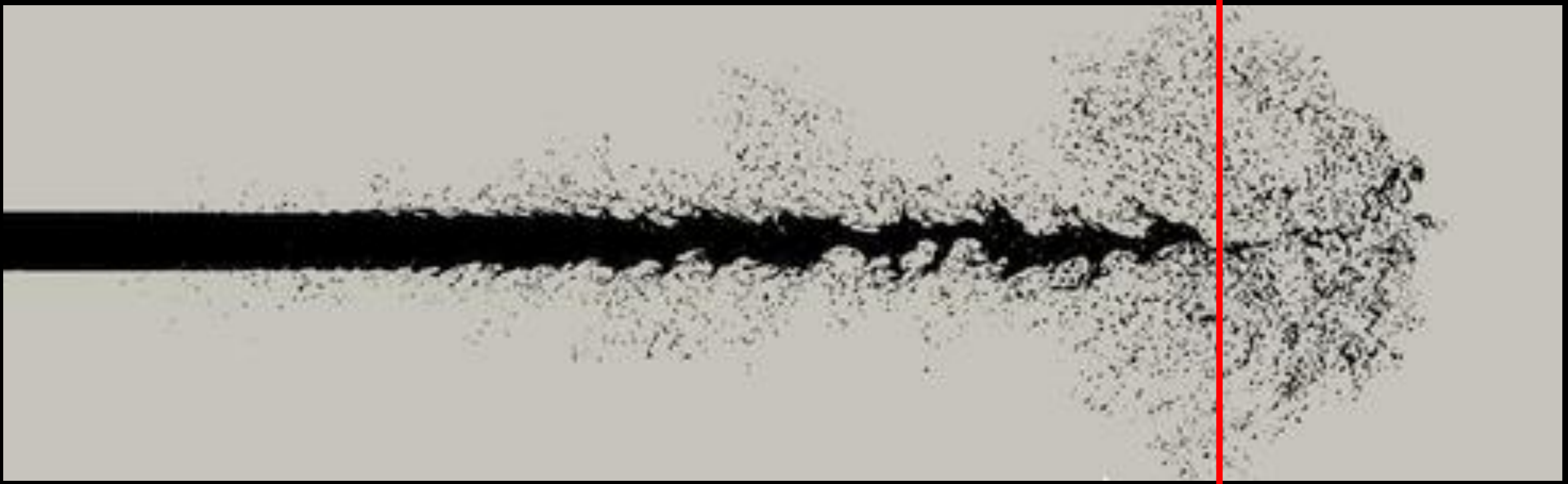
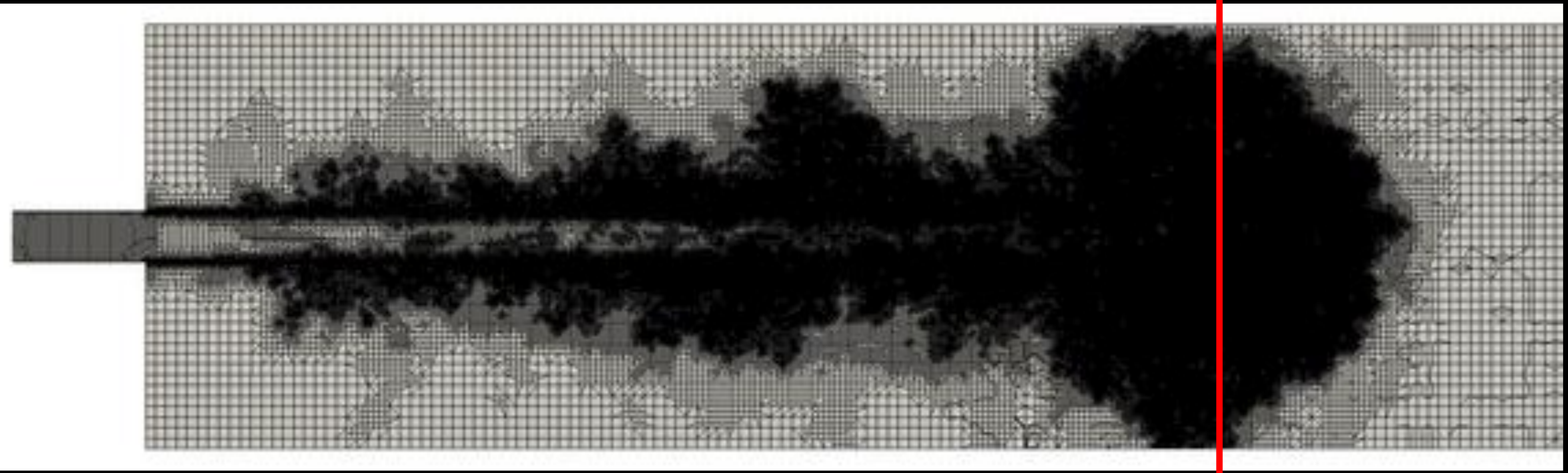
*Time: 0.1  $\mu s$*

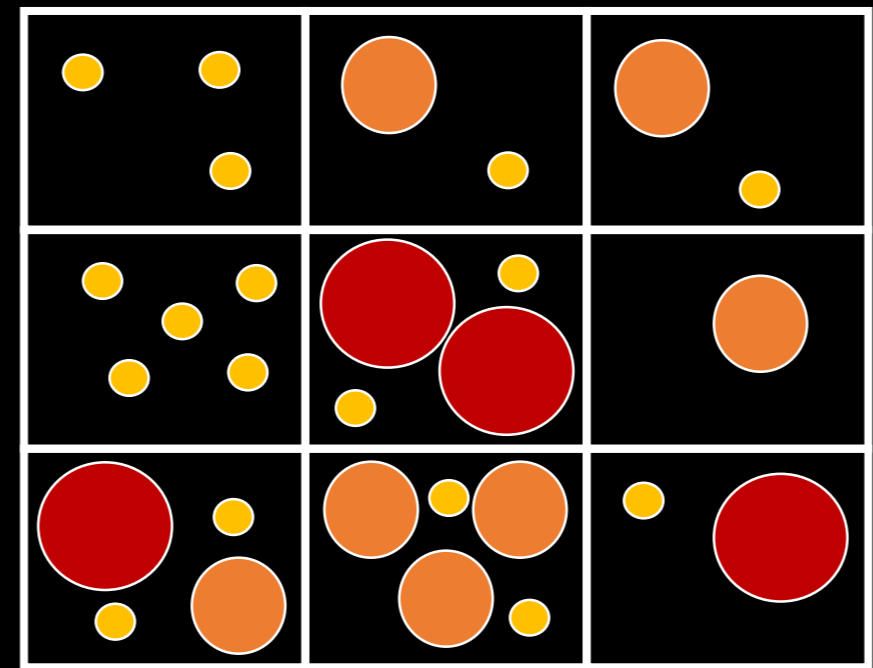
## n-dodecane at 150MPa



- Base cell size is 40 microns
- Four refinement levels are used, yielding 2.5 microns near the interface
- Grid is pre-refined near the interface and in the nozzle
- Started from 0.7M cells and ended up with 133M cells







# Euler-Euler



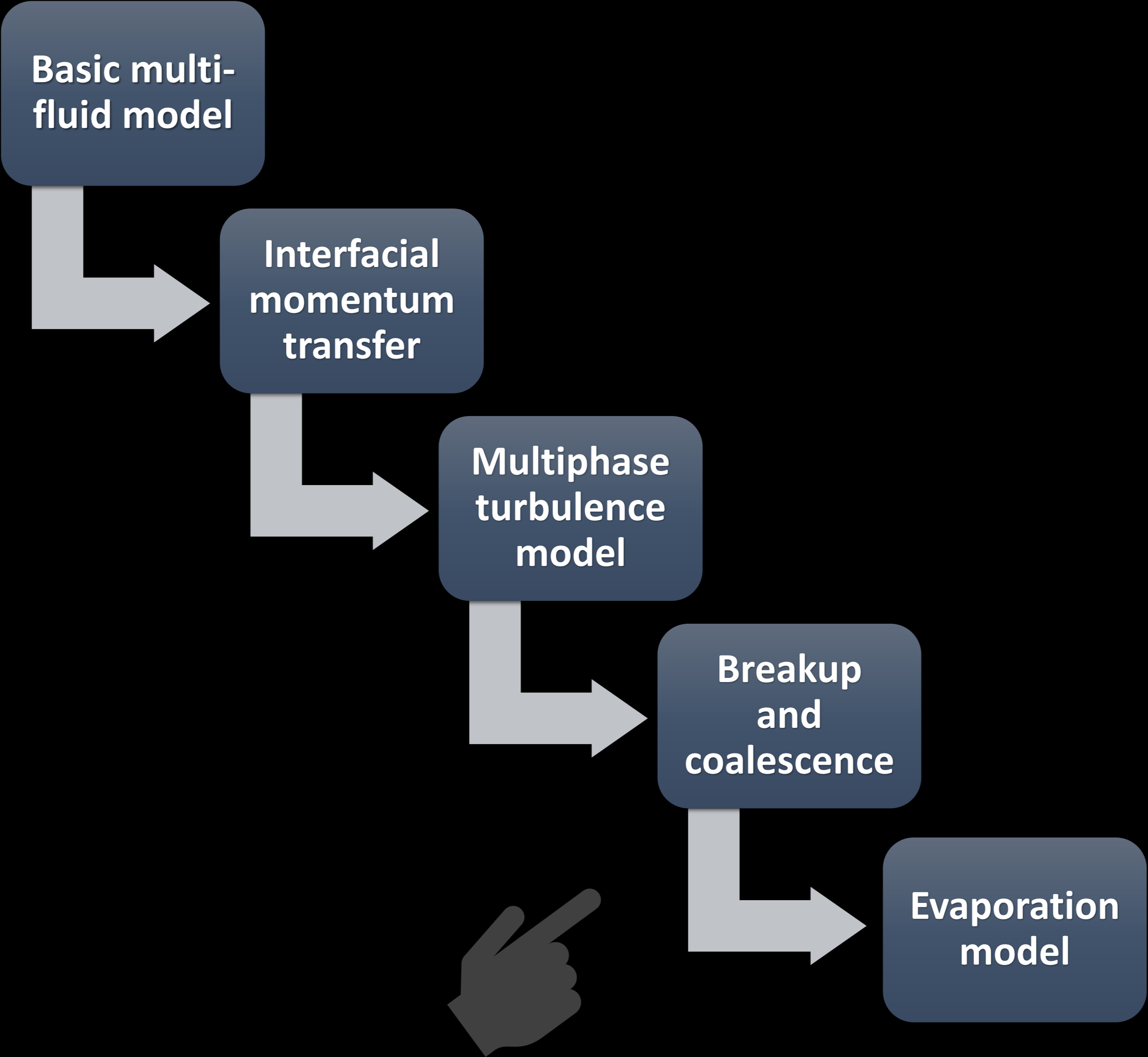
# Euler-Euler solver

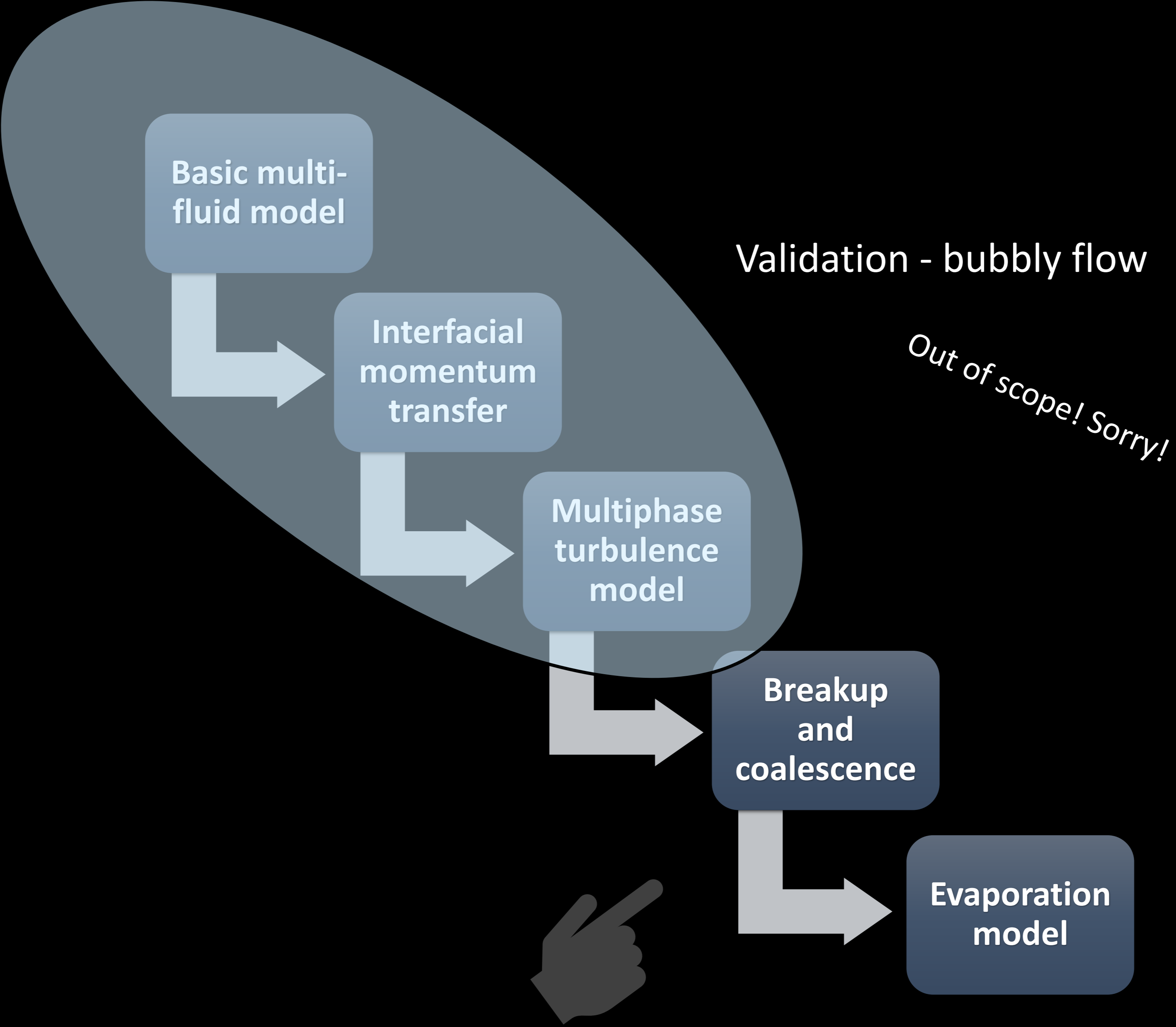
- Incompressible multi-fluid solver for polydisperse flows
  - multi-fluid – two-phase, but arbitrary number of droplet classes
  - method of classes in the Euler-Euler framework
  - polydisperse – droplets can vary in size
  - every class has a momentum and phase continuity equation
  - mixture pressure assumption – all phases/fluids share the same pressure equation

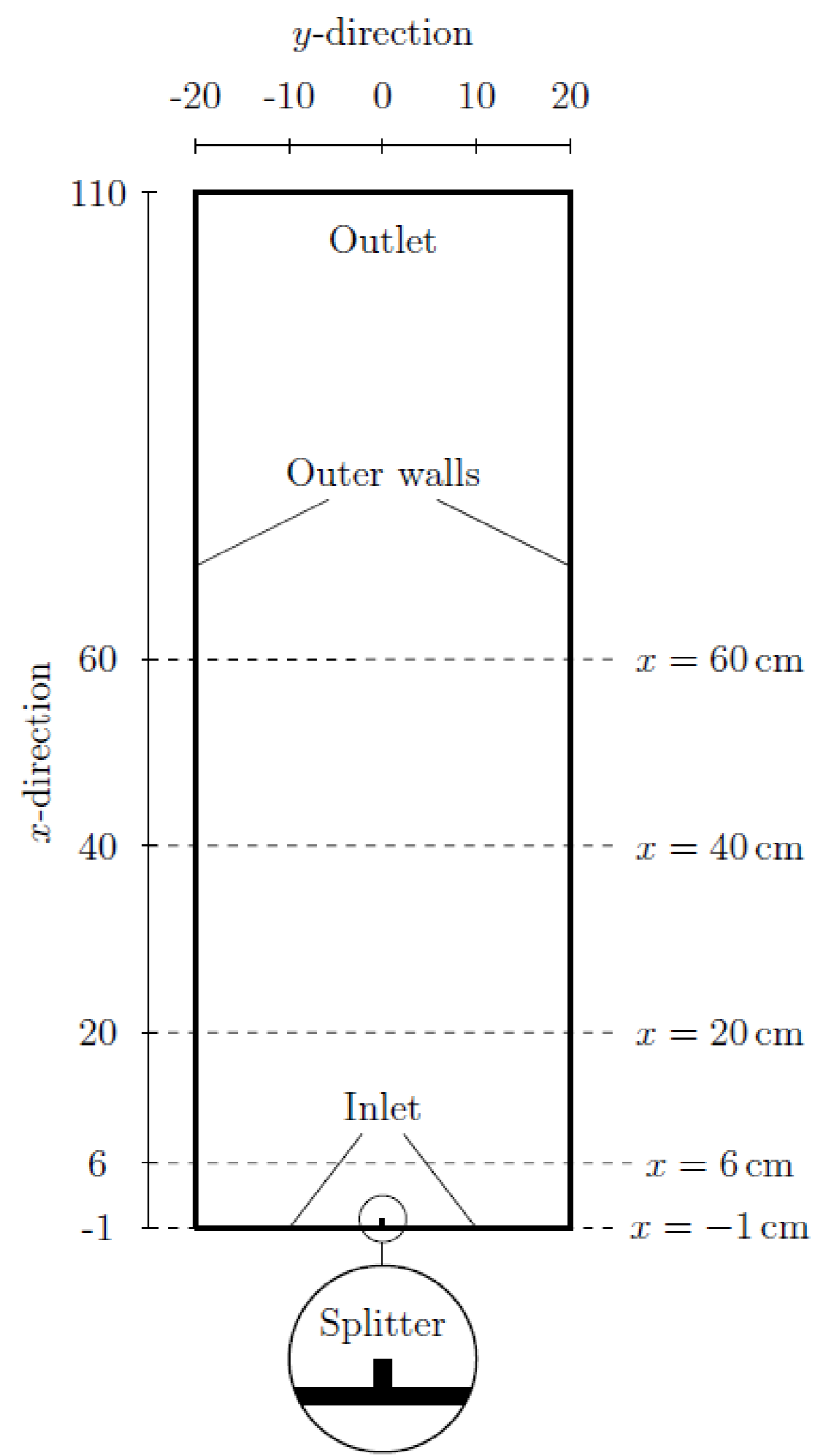


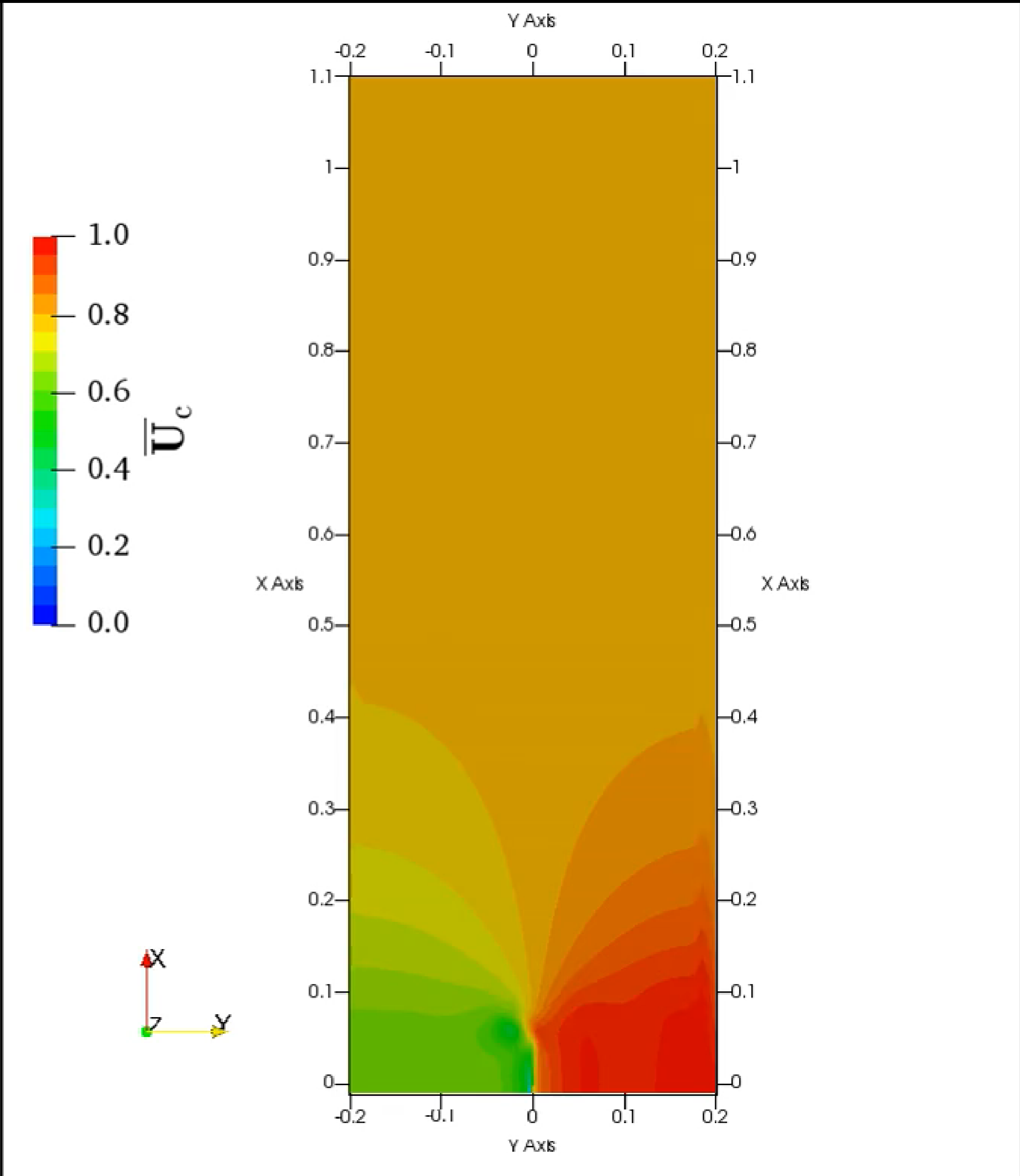
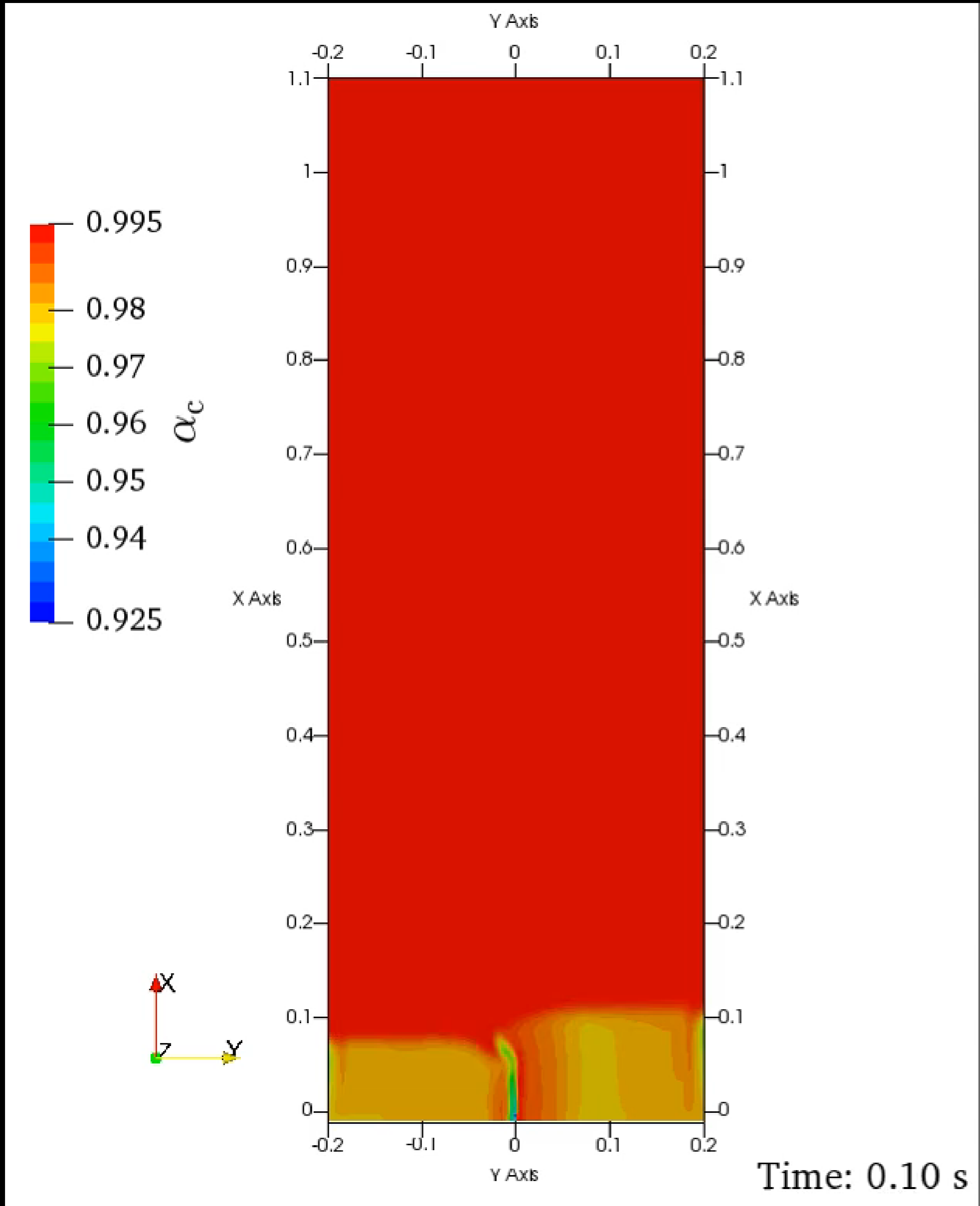
# Euler-Euler solver

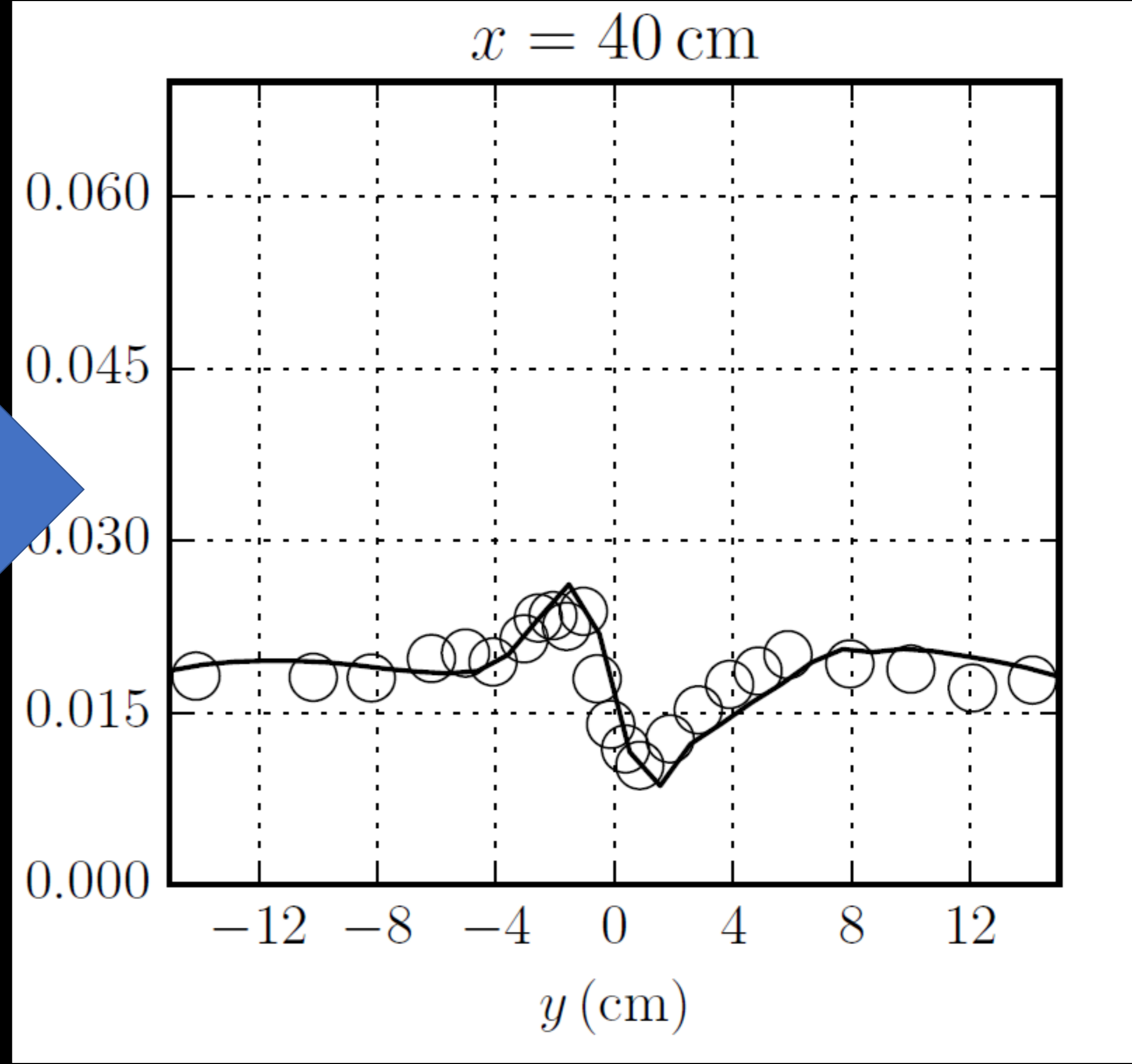
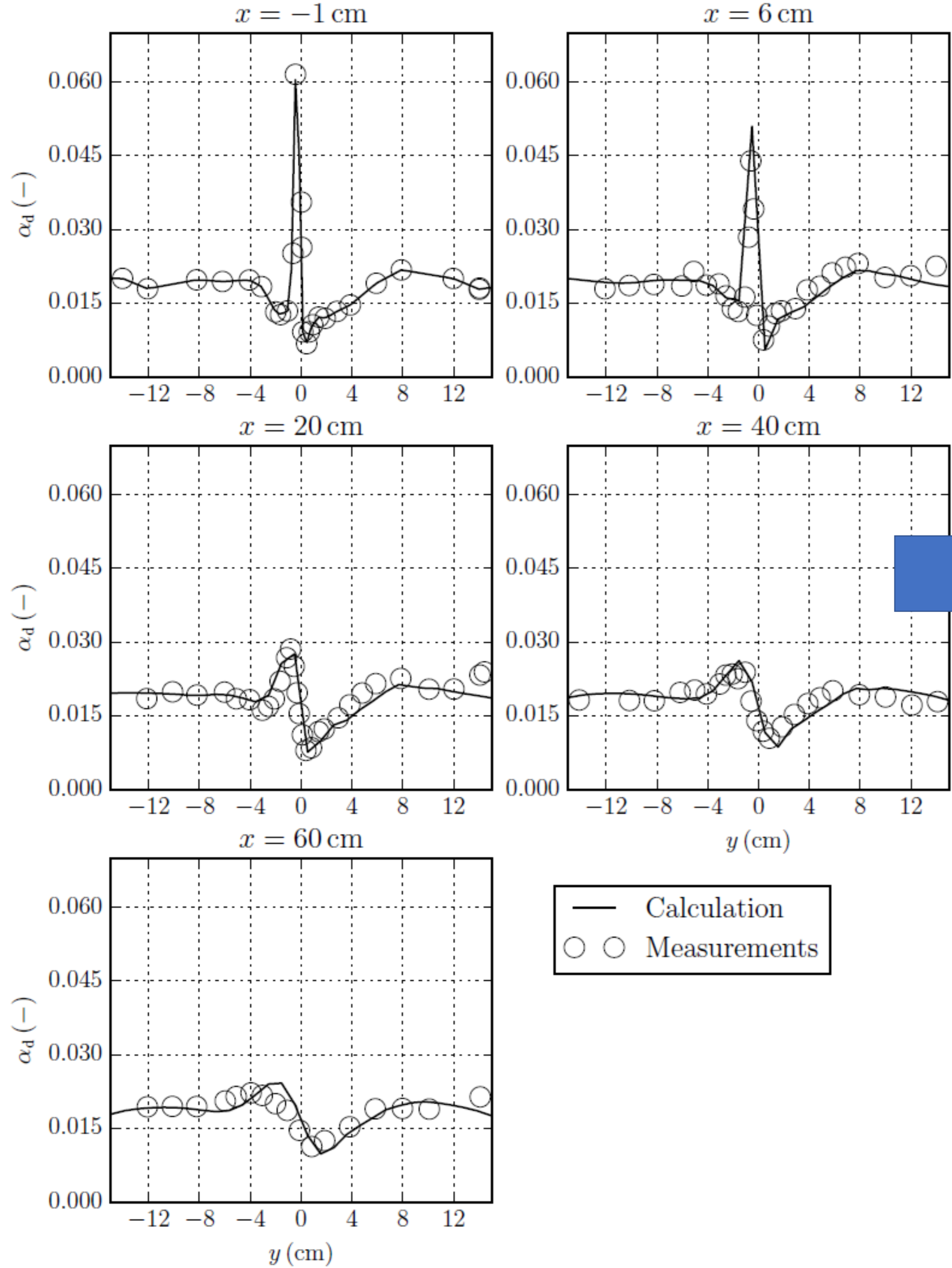
- Inter-facial momentum transfer
  - Drag, lift, virtual-mass, turbulent dispersion force (~~wall-lubrication~~)
- Mixture  $k - \epsilon$  turbulence model (generalised for multi-fluid)
- Breakup and coalescence functionality

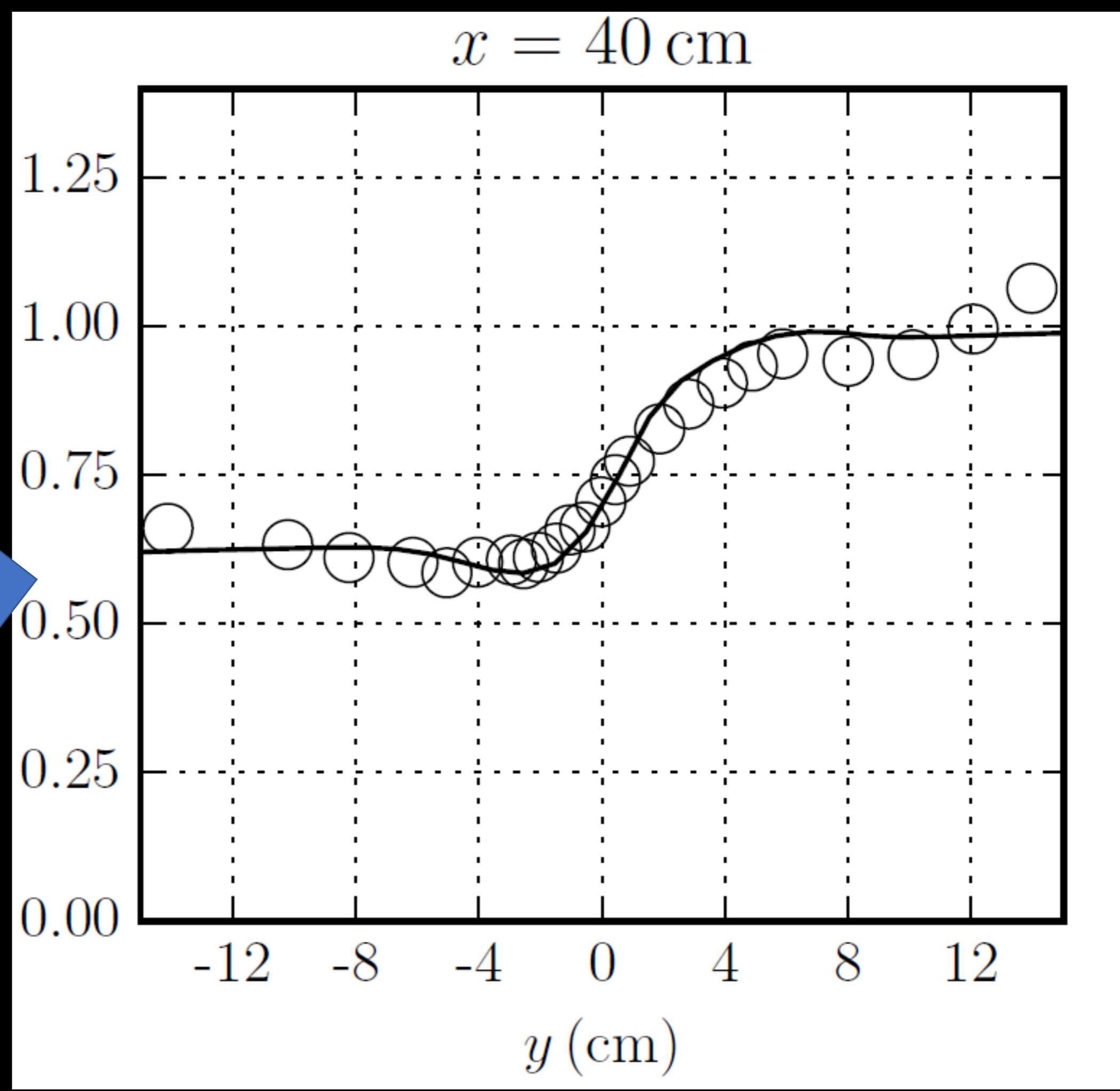
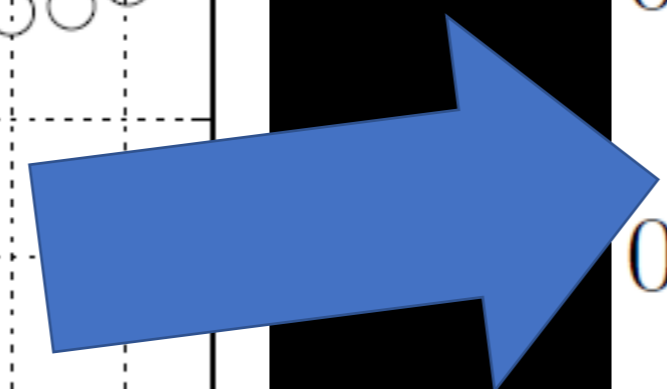
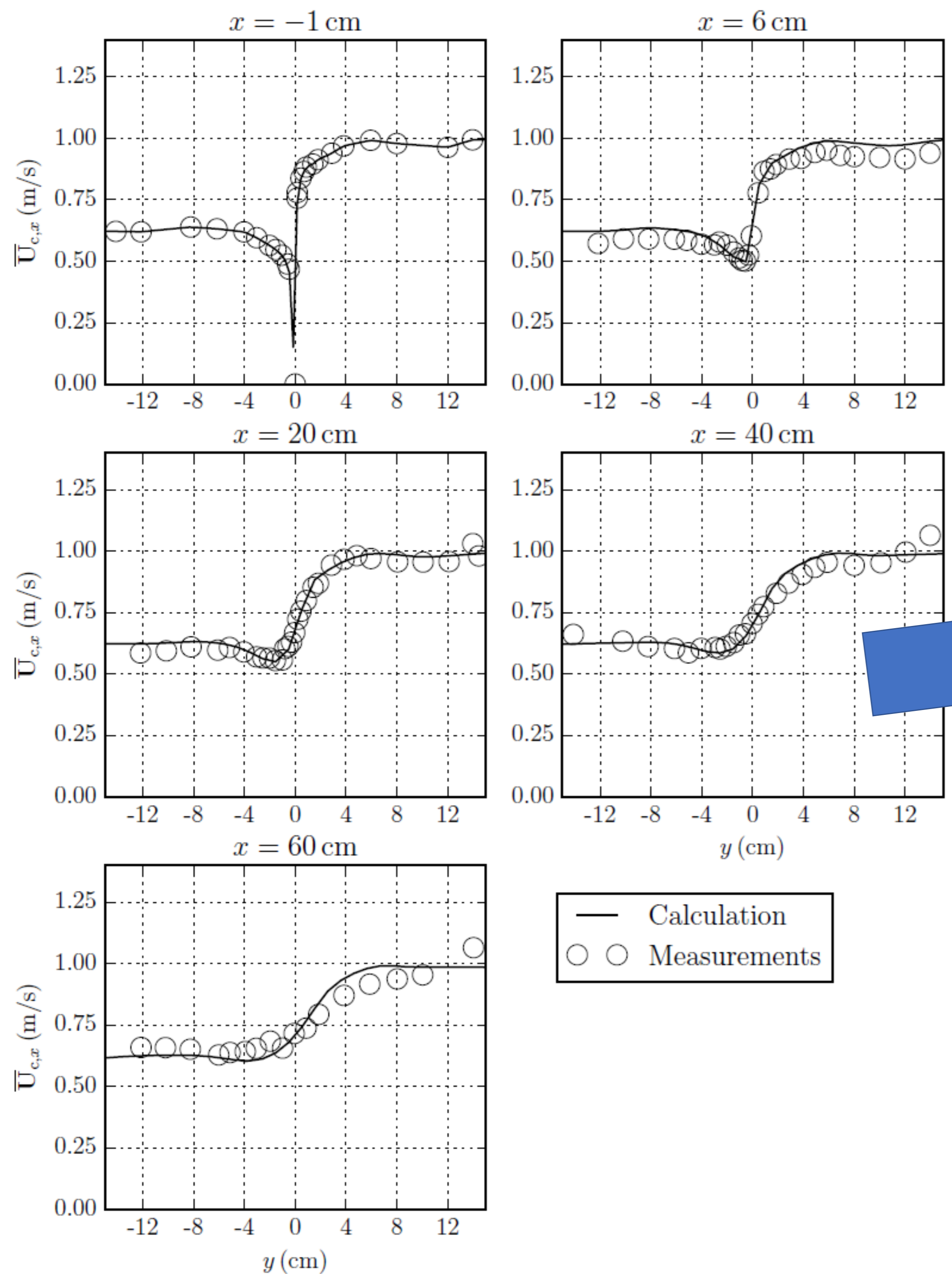


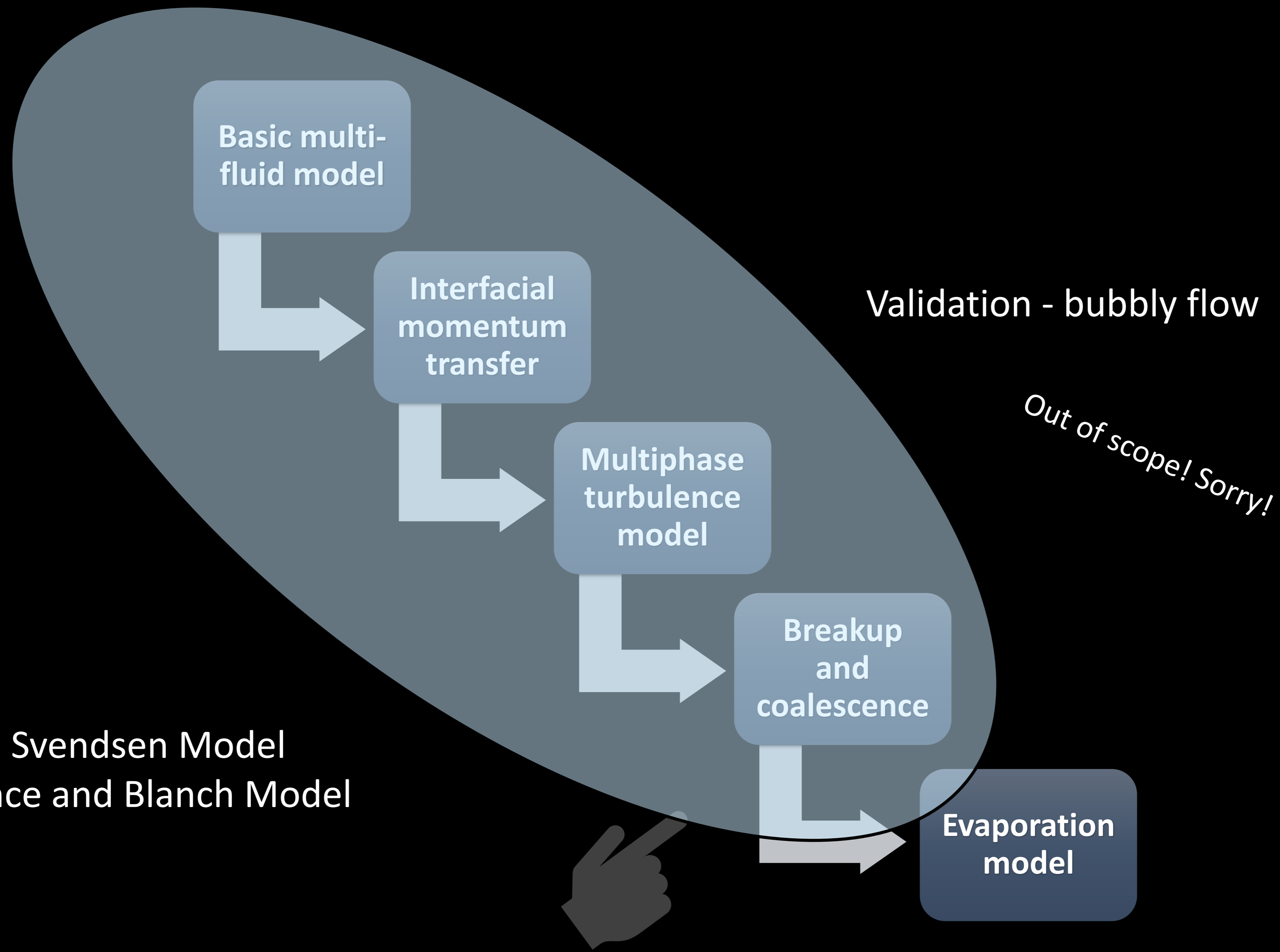








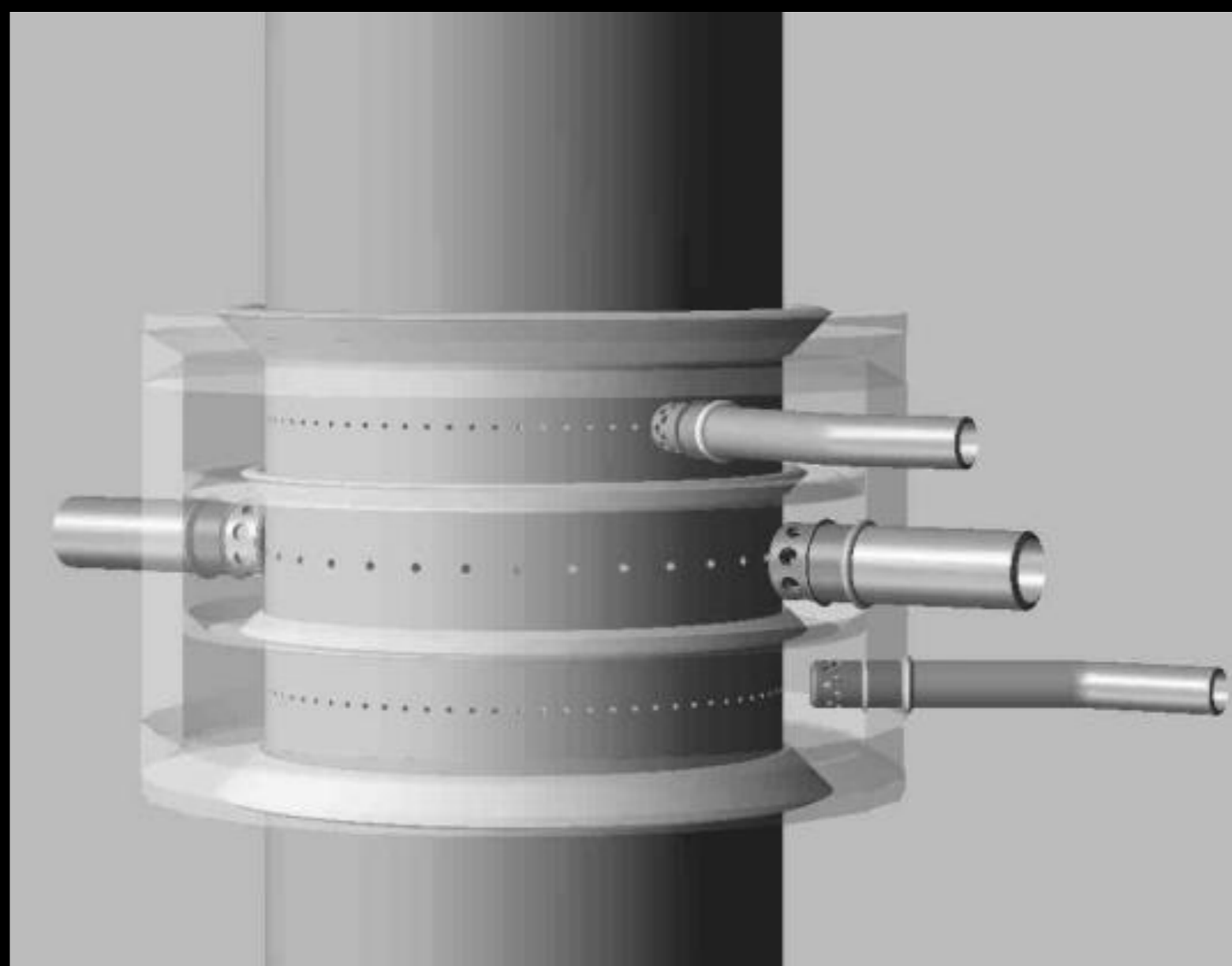
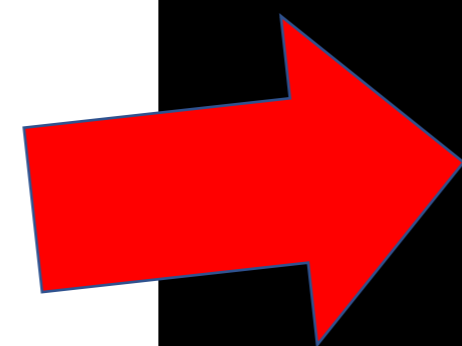
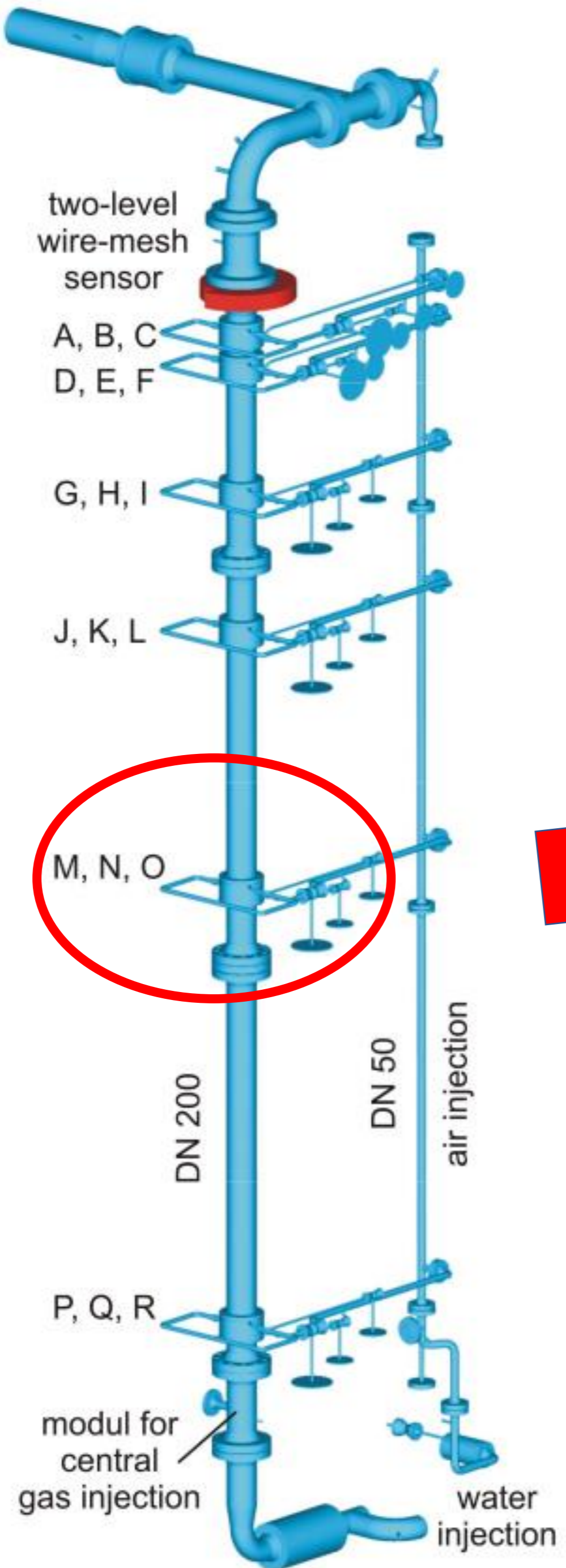


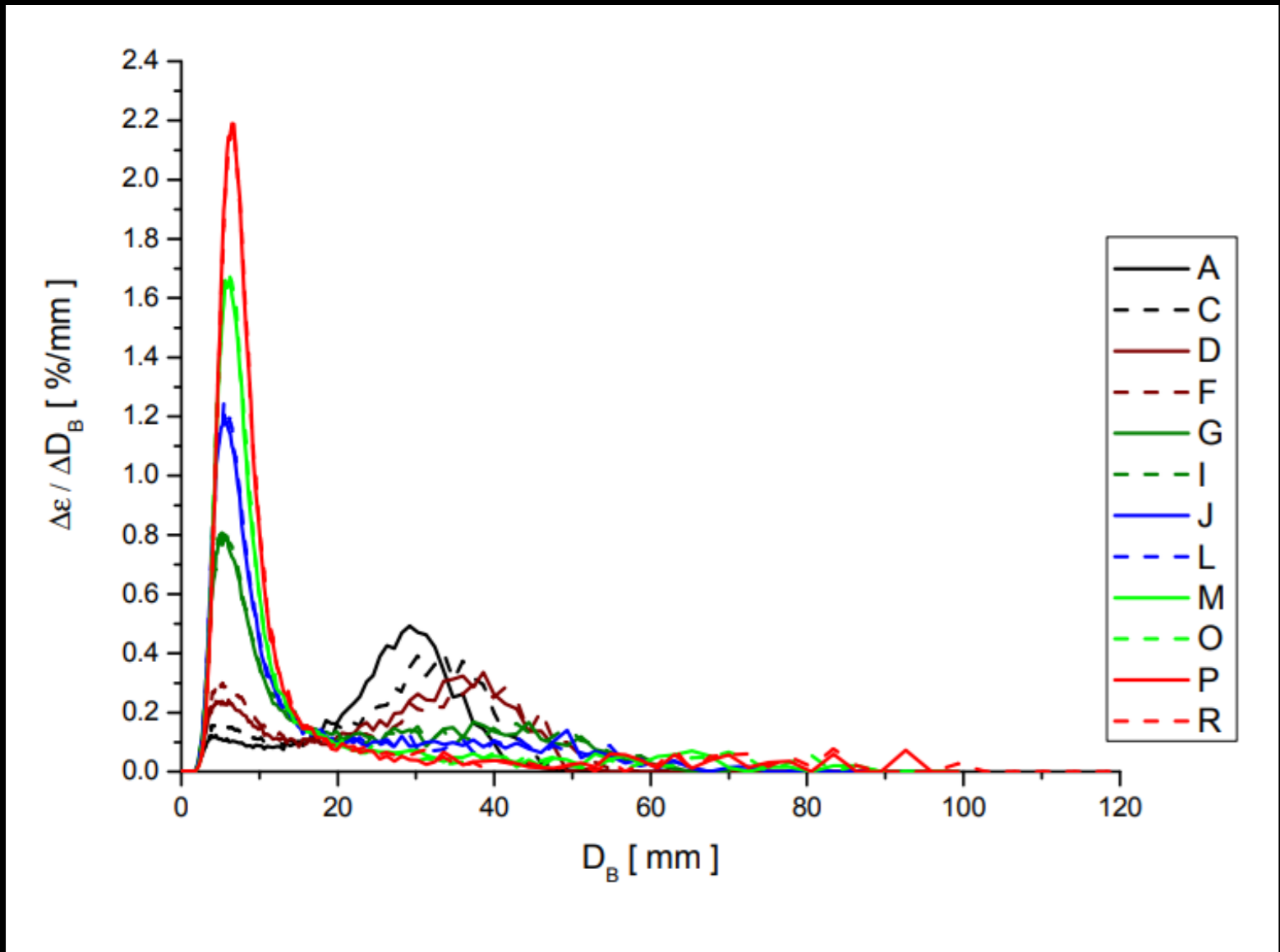
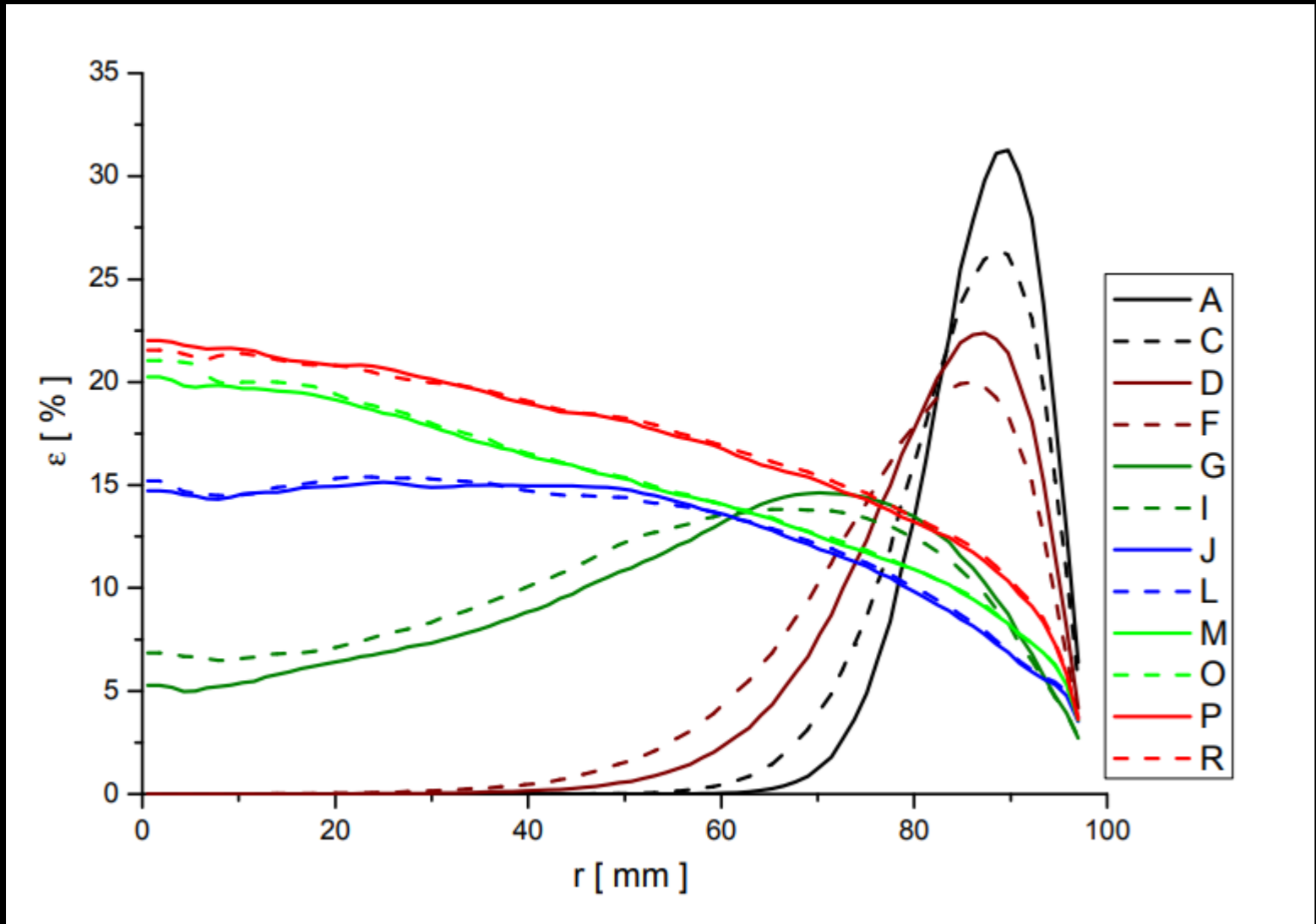


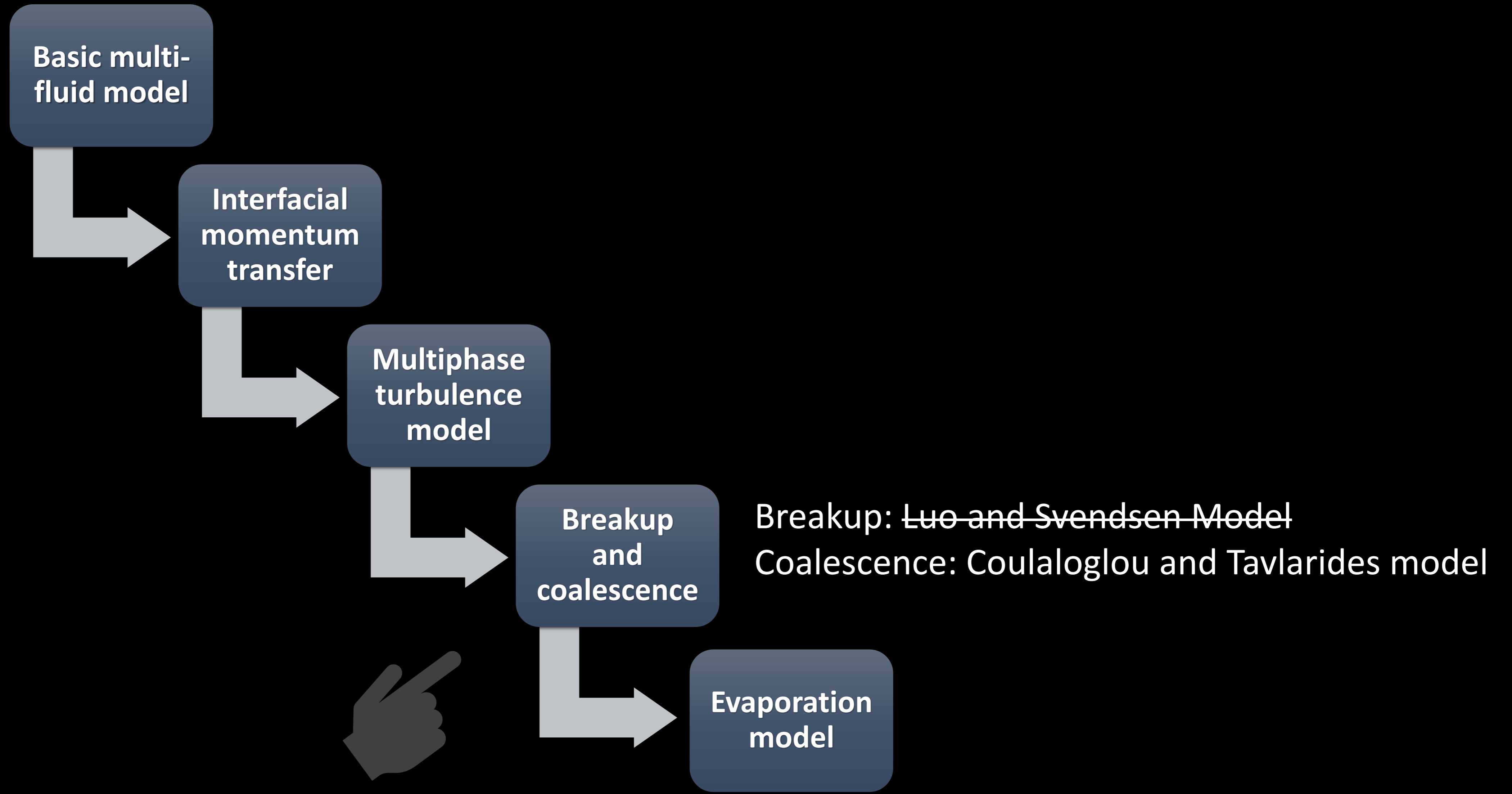
Breakup: Luo and Svendsen Model  
Coalescence: Prince and Blanch Model

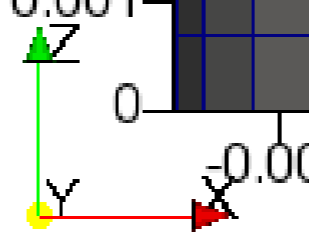
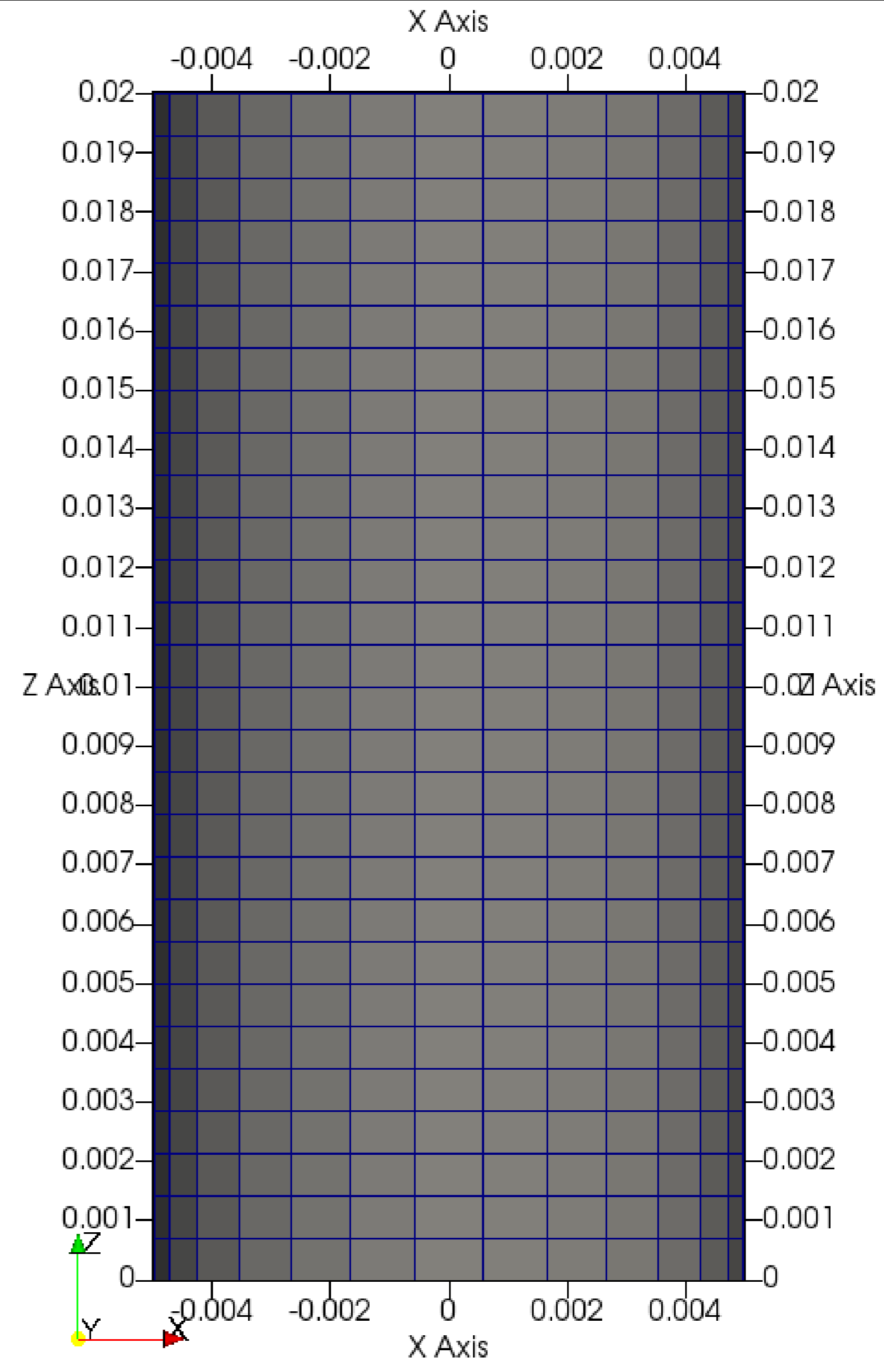
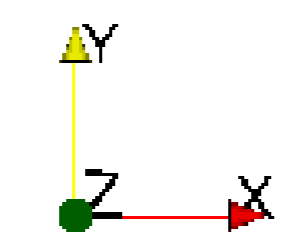
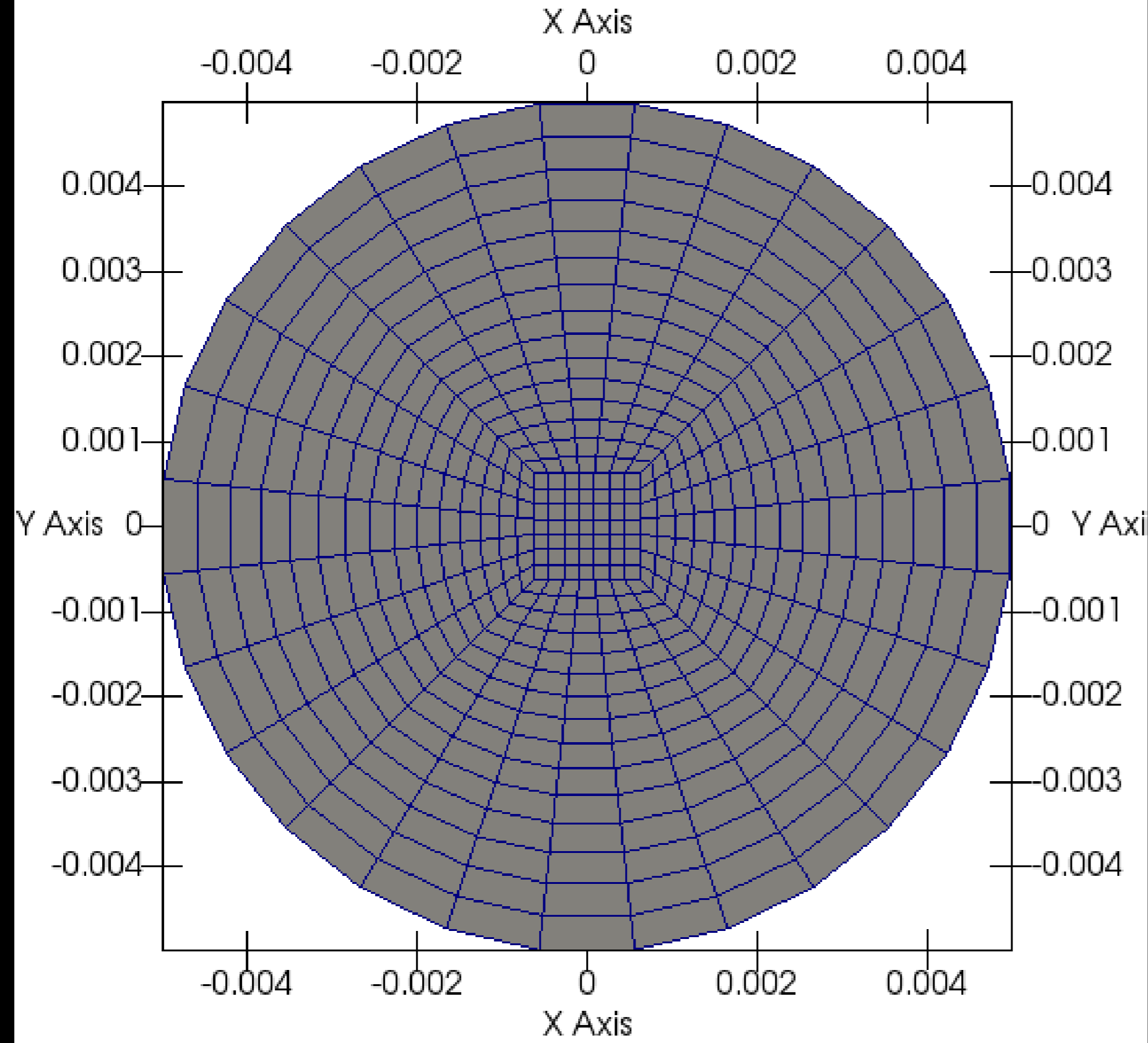


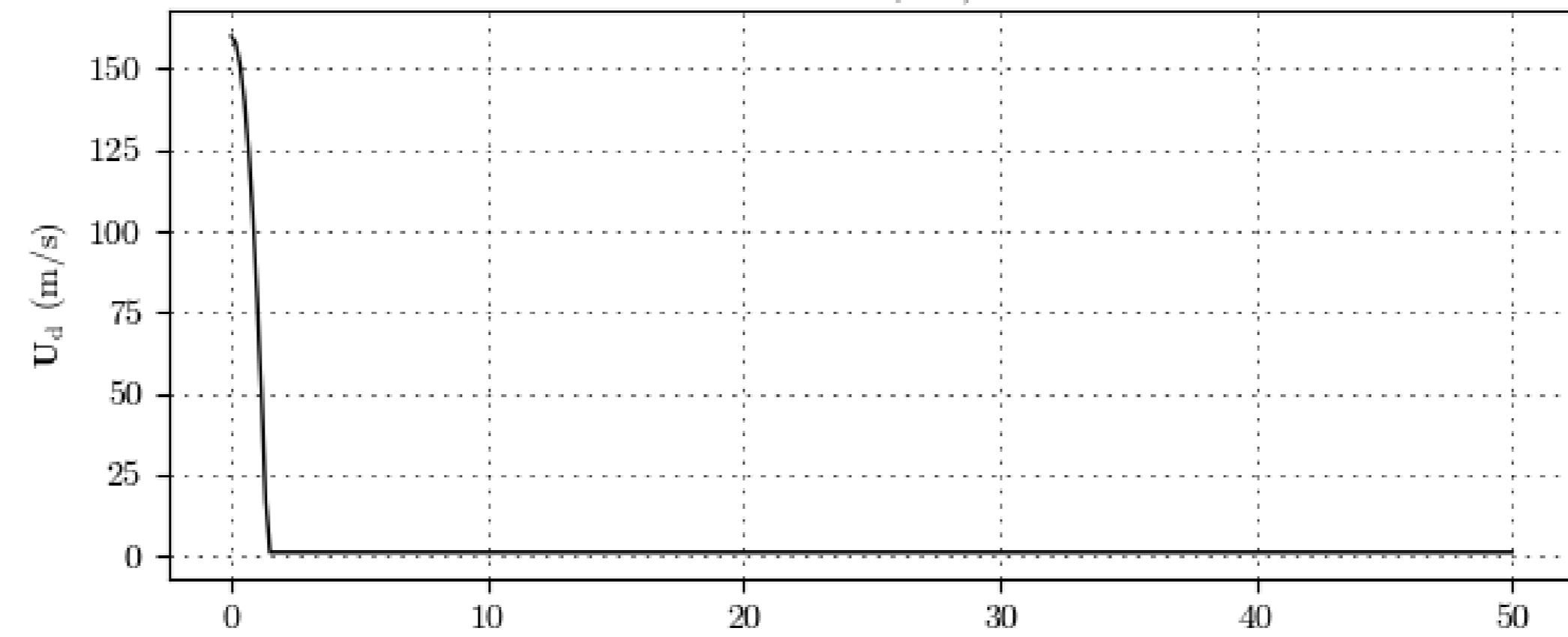
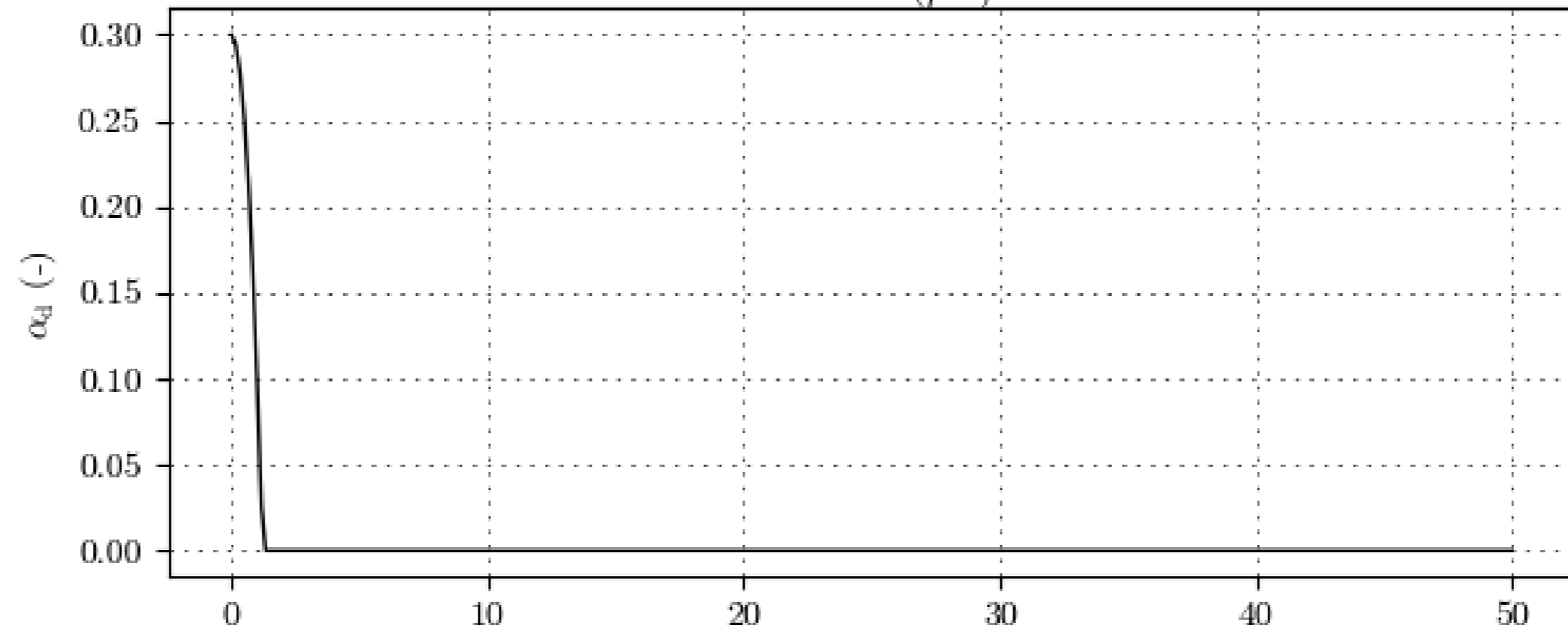
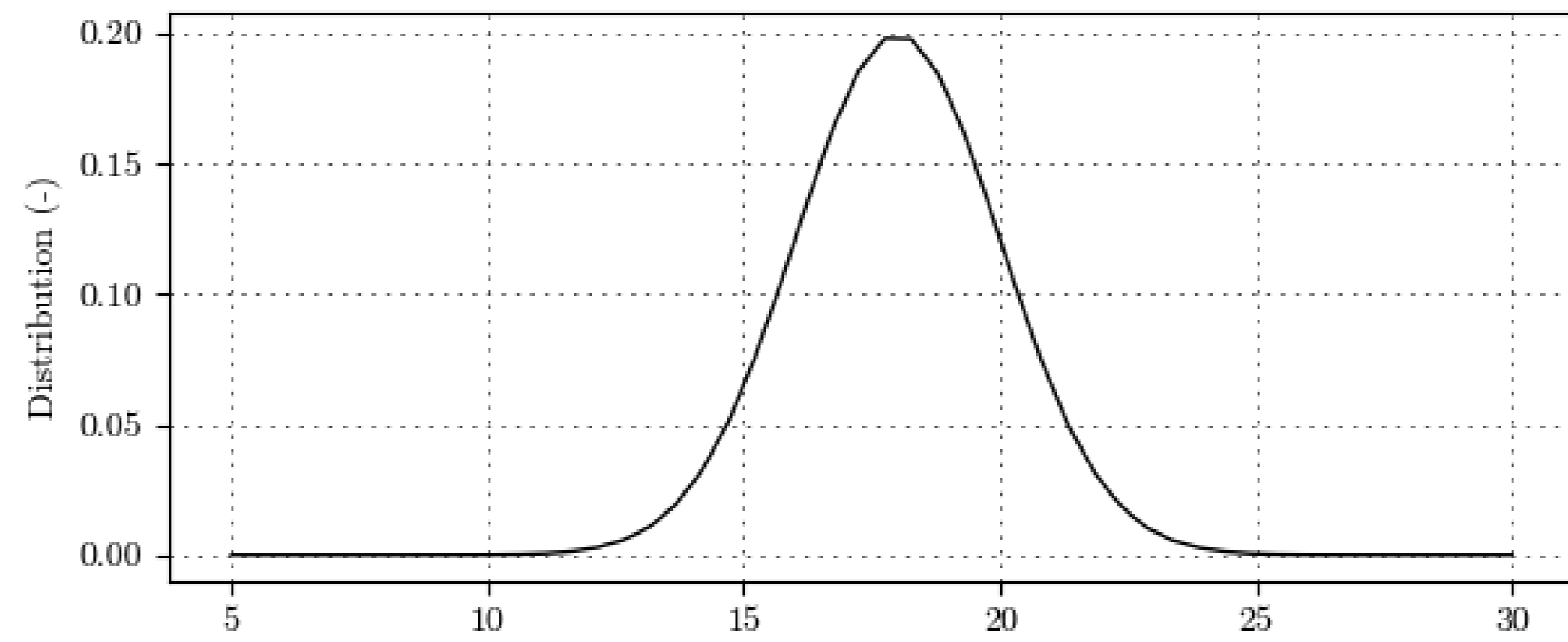
# TOPFLOW (Transient Two Phase Flow Test Facility.)

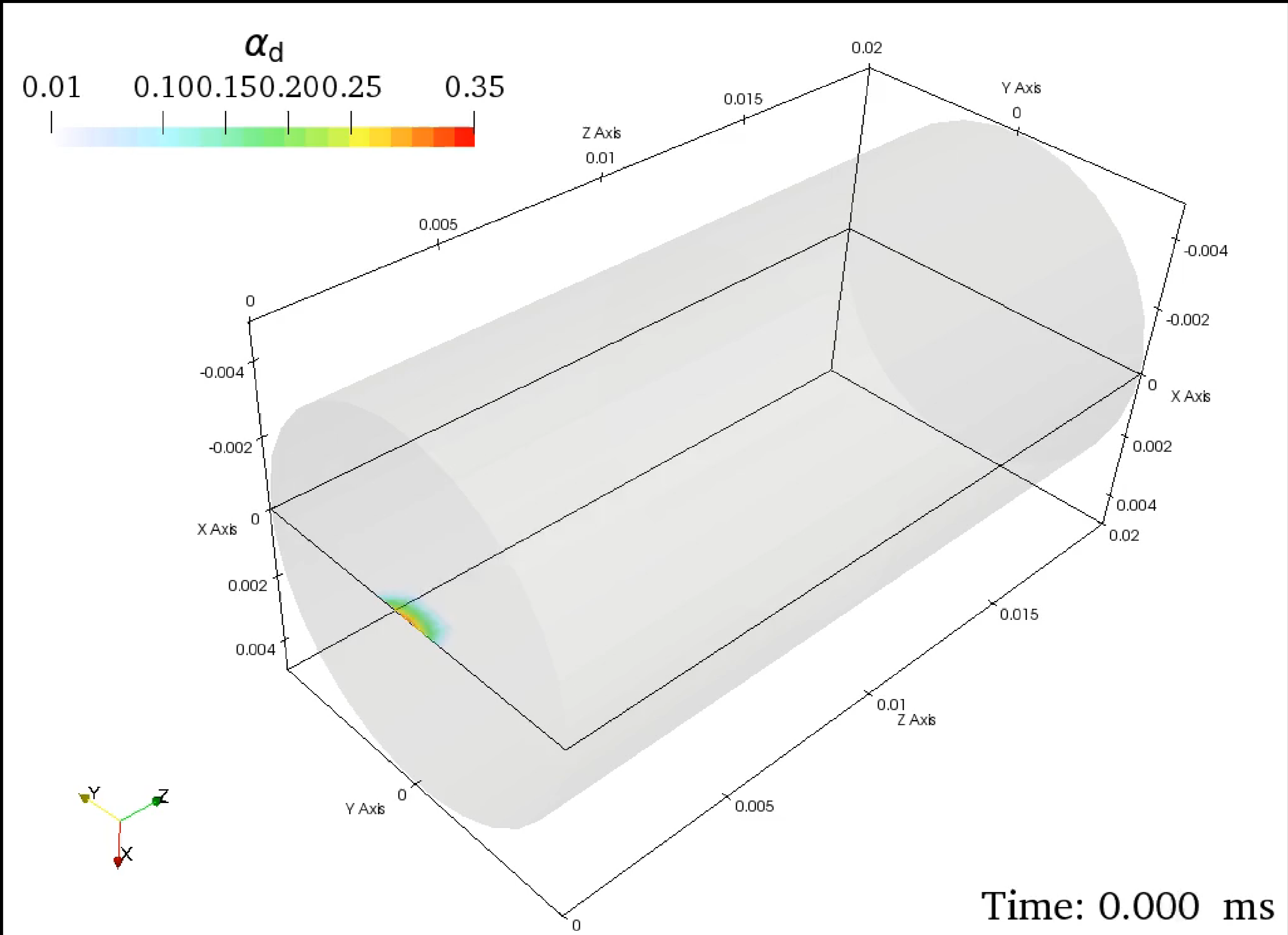


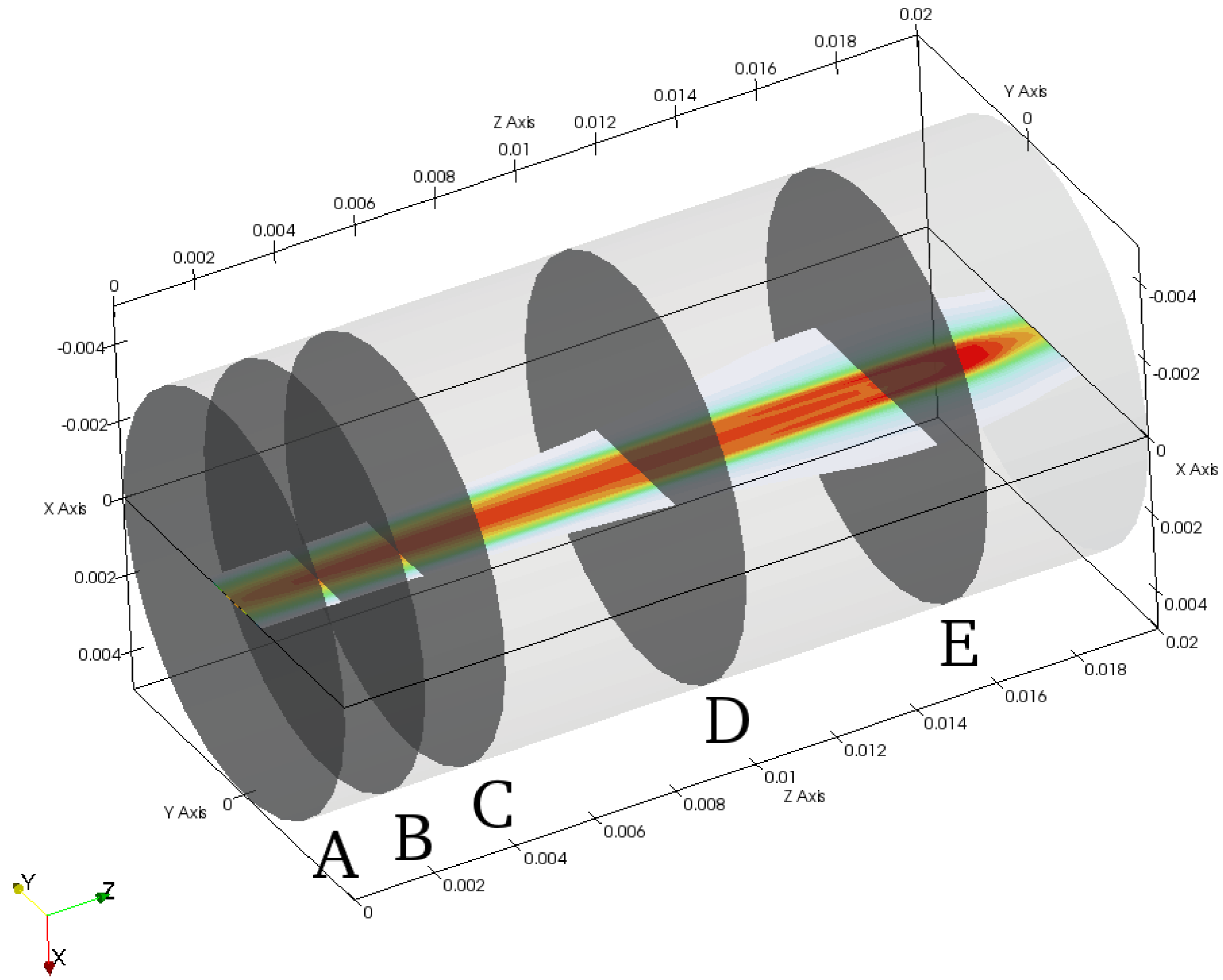


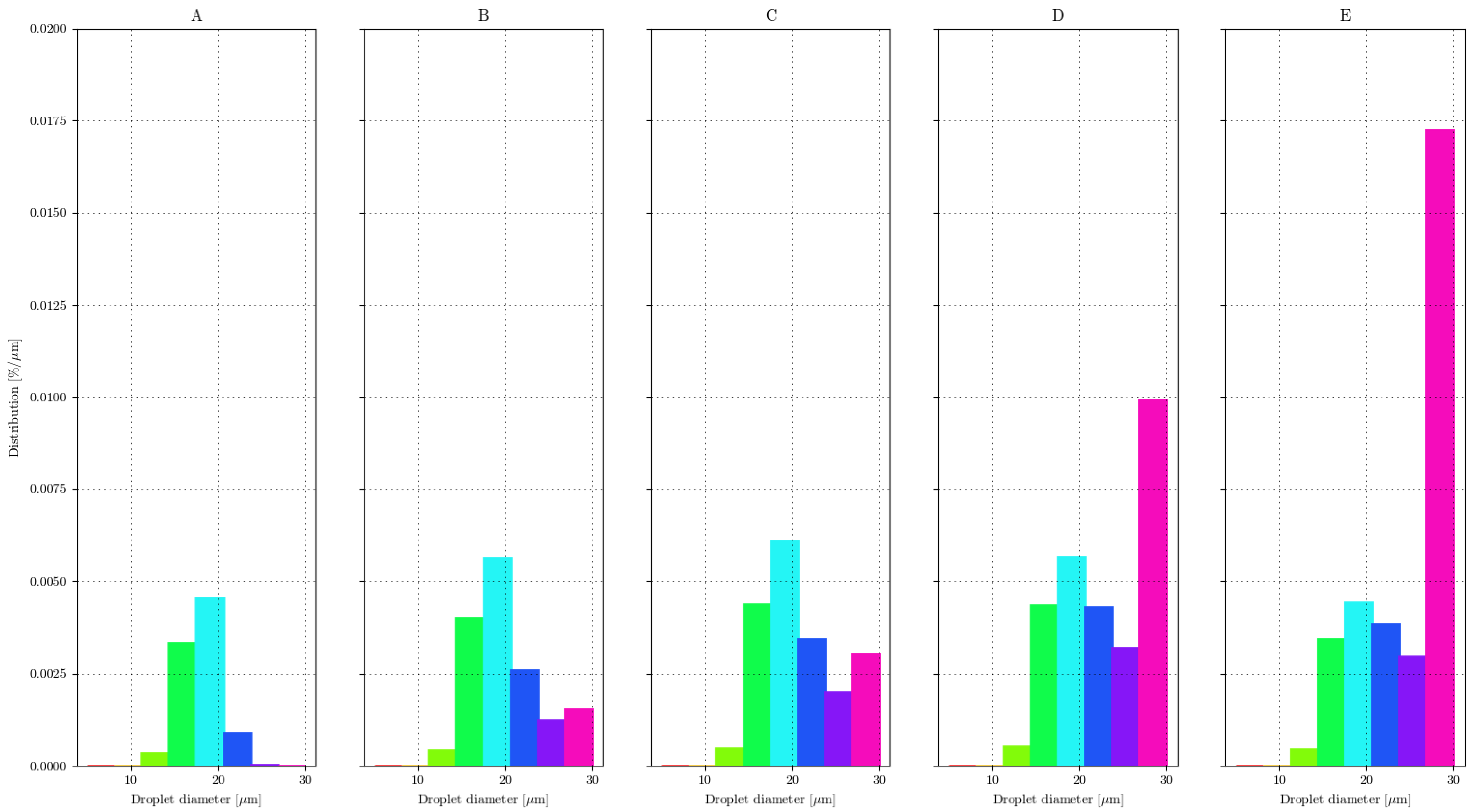




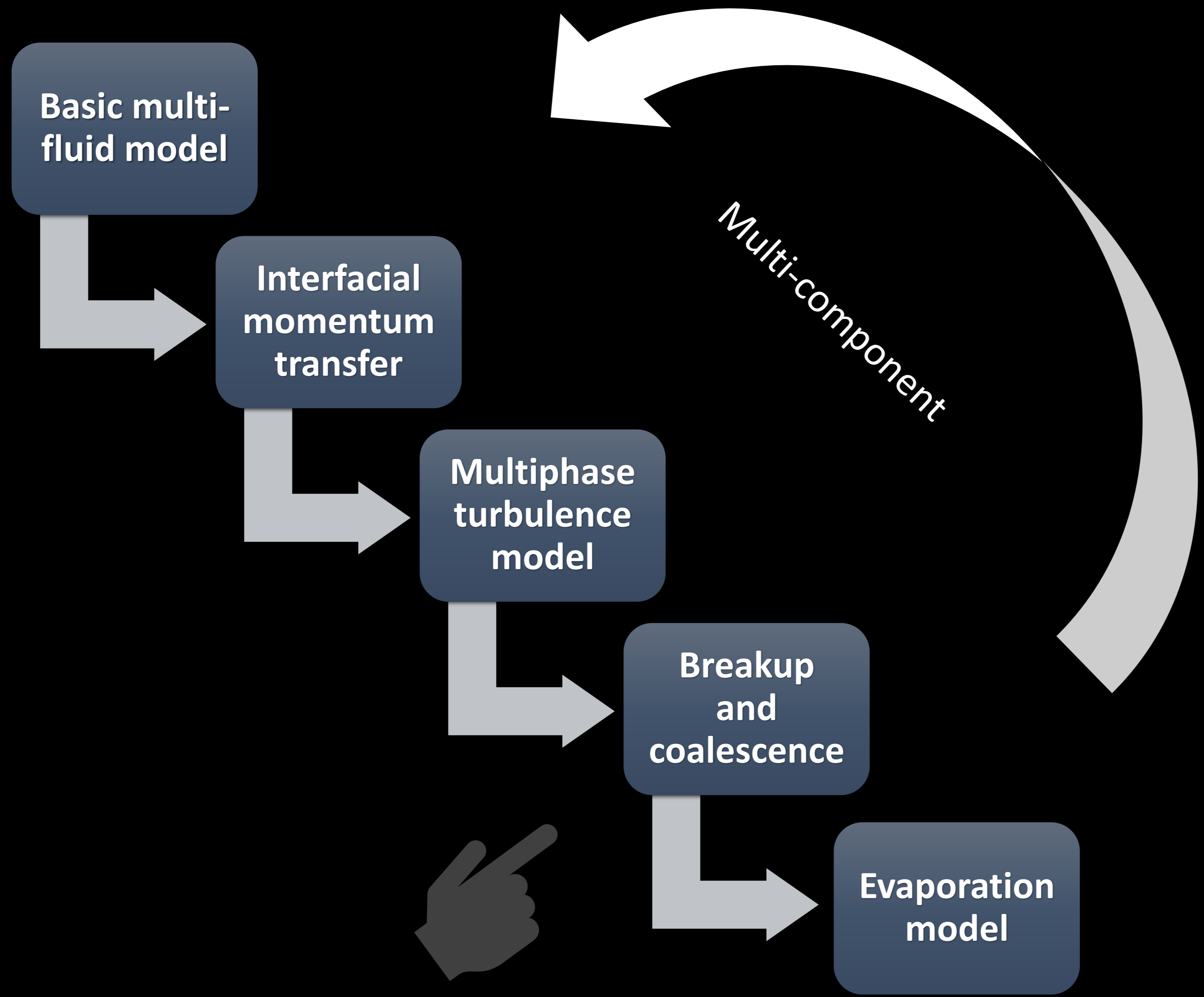












# Acknowledgements



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# Questions?

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